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An Analysis of How the Payload and the Speed Affect the Repeatablility of the Microbot Teachmover Robot

Abstract

With the increasing application of robots to many fields in our life, the accuracy and the repeatability of robots become more and more important. Many applications require robots to have high repeatability and accuracy. There are many factors which can affect the repeatability and the accuracy of a robot.

This study was to examine how the two key factors of payload and speed affect repeatability. The experiment was conducted in the CAM Laboratory of the Industrial Technology Center, University of Northern Iowa, by using Microbot TeachMover. Six different payloads: 2gm, 20gm, 65gm, 130gm, 180gm and 250 gm, and three different speeds: speed(3), speed(5) and speed(?) were exerted under the control of the same program. The robot with certain payload and speed ran 30 cycles, and the spatial positions were measured by three dialindicators which represented three-dimensional coordinates (X,Y,Z). After the data were collected, the relative spatial position deviation was calculated. The first cycle point was used as the original position. The researcher used the mean of the spatial position deviation and the range of spatial position deviation to analyze the affect of payloads and speeds on repeatability. Also linear trend "b" and the coefficient of correlation "r" were used to identify repeatability change during the 30 cycles. Analyzing the collected data led to the conclusion that light payload and medium speed have better repeatability, and both higher speed (7) and lower speed (3) lead to lower repeatability.

AN ANALYSIS OF

HOW PAYLOAD AND SPEED AFFECT THE REPEATABILITY OF THE MICROBOT TEACHMOVER ROBOT

A Research Paper Presented to the Graduate Faculty of the Department of Industrial Technology University of Northern Iowa

In Partial Fulfillment of the Requirement for the Non-Thesis Master of Arts Degree

by

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Date: February 4, 1992

Approved by:

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Feb.

Date

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ABSTRACT

With the increasing application of robots to many fields in our life, the accuracy and the repeatability of robots become more and more important. Many applications require robots to have high repeatability and accuracy. There are many factors which can affect the repeatability and the accuracy of a robot.

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CHAPTER I

INTRODUCTION

Since the robot entered our life, it has become more and more important. Industrial robots can be found anywhere producing many products we use and doing many boring jobs that people do not like to do.

Robot applications are continuously widening, and their functions are becoming more and more powerful, but many problems with using robots and with the design and function of robots still exist today. People expect robots to work perfectly. Robots need to meet people's high requirements.

Industrial robots have typically been used as general purpose positioning devices. In such a situation, the robot is programmed to move through a sequence of positions so that a tool or part held by the robot completes a desired task on a workpiece, whose position is already set in relation to that of the robot. The most important requirement for successful accomplishment of its task is the repeatability with which it can return to the taught

positions and with which successive workpieces can be presented to it (Taylor, 1985).

Some manufacturing operations, such as welding, deburring, routing and scanning, require the robot to move a tool in a continuous path. Therefore, kinematic measurement of accuracy and repeatability that test the robot's ability to trace accurately a path through its workspace at a rapid pace are far more important for these operations (Tracking system measures continuous path robot motions, 1985).

Most of the tasks need the robot to execute with high accuracy. "Accuracy of robots is required in an increasing number of applications" (Day, 1988, p. 1). Day (1988) said, "It is important for users of robots to understand factors affecting accuracy [and repeatability] and where present technology stands in making accuracy [and repeatability] improvements" (p. 9).

A major goal of robot research and development over many years has been finding techniques for improving the effective accuracy or repeatability of the manipulator, i.e., the precision with which it can place a part or tool at a fixed position relative to a

workpiece. Calibration methods and equipment sensing methods are the major approaches for such a problem (Taylor, 1985).

This study will use an experimental method on a Microbot TeachMover Robot to identify some important factors affecting the repeatability of a robot. The effect of payload and speed on repeatability will be determined.

This laboratory research can explore a way for researchers to make a significant study on industrial robots, and provide more information for industrial robot designers to improve the quality of robots. This study can also make up for a shortcoming of specifications on the basic parameters of the Microbot TeachMover Robot -- repeatability.

Purpose of the Research

The purpose of this study was to:

- Identify key factors that can affect the accuracy and repeatability of the Microbot TeachMover robot.
- Analyze an important characteristic -- repeatability
 -- as the dependent variable in a study of the Microbot TeachMover robot.

3. Gain more knowledge about industrial robots from the study of a robot in an educational laboratory.

Research Problem

There are various factors which may affect the repeatability of a given robot. The problem of this research was to determine how the factors of payload and speed affect the repeatability of a Microbot TeachMover Robot (MTMR).

Research Ouestions

The research questions of this study were:

- 1. How does the weight of payload affect the repeatability with a certain speed in terms of "QD" and "R"? "QD" is the mean of spatial position deviation of the thirty cycles; "R" is the range of spatial position deviation of the thirty cycles. Six different weights of payload were applied.
- 2. How does the speed with a certain payload affect the repeatability in terms of "@D" and "R"? Three speeds were tested.
- 3. How does the spatial position deviation "@D" change during the thirty cycles in regard to the

analysis of "b" and "r"? "b" is the changing rate of "@D"; "r" is the coefficient of correlation.

 How does @D change when the robot run more than 30 cycles. The payload 65 with speed 5 and 7 was applied under 50 cycles.

Significance of the Research

Robots have a large number of applications. They are generally flexible, reprogrammable and repeatable from cycle to cycle. However, for many new industrial applications in which high repeatability and accuracy are required, the current accuracy and repeatability can not satisfy these high requirements. The robot needs to be more accurate and more repeatable, and the physical location or trajectory reached by the endeffector must be precisely where the robot has been directed (Day, 1988).

The importance of a robot's accuracy and repeatability was recognized in the early years of robotics development, and it has taken some time for the necessary technology in manipulator development, sensor development, and application development to realistically and economically overcome robot

inaccuracy and poor repeatability. But we have not quite reached a stage when robots can be produced accurately within desired cost (Day, 1988).

By conducting this research, the factors which can affect the repeatability and accuracy of a robot will be carefully investigated and more valuable data will be collected and analyzed. As a result of this research, the researcher will supply some important information which can be used by robot designers to improve the quality of a robot.

The Microbot TeachMover Robot will be used in the laboratory for this research. The current instruction manual for the Microbot TeachMover Robot lacks information about the accuracy and repeatability in its specification list. This research can remedy this defect and make it better for future educational use.

Delimitations

This study was limited as follows:

 This research was conducted in the CAM Laboratory at University of Northern Iowa. The Microbot TeachMover robot which was used for this research had been used for about five years. Its accuracy

might not maintain the same level as a new one.

- The research used the teach pendant to program the robot. Only payload and speed were considered without considering other factors.
- Three dial-indicators were used to measure the spatial position deviation on X, Y, Z axis separately. Resolution of the Dial-Indicator is .001 inches.
- 4. Repeatability was studied in regard to the analysis of the relative spatial position deviation. A robot with certain payload and speed was run 30 cycles under the control of the same program.

Assumptions

This study had the following assumptions:

- 1. All the tests were not affected by environmental conditions.
- 2. There was no reading error during the measuring process.
- 3. There was no slippage between payload and gripper, robot and table as well as dial-indicator set-up and table. The table on which all tests were carried out did not shake during the test.

Definitions

The following terms were defined for this study:

- 1. The Microbot TeachMover Robot -- A small "educational" robot developed to help researchers and students learn about robots, with a low cost machine that fully simulates the large industrial machines (Heath, 1986).
- 2. The Teach Pendant -- A special command module used to command the robot to memorize points along the path of motion. It can also set timers to synchronize the operation, command the sensing of external inputs, and dispatch output signals to peripheral process equipment (Asfahl, 1985).
- 3. Payload--Weight of the object handled by the robot.
- 4. Robotic programming -- A key feature of robots which have capability for being reprogrammed for different tasks. There are many methods of programming. Teach pendant is one of the manual controller methods.
- 5. Repeatability--The ability to return to the same spot again and again after that point has been specified.
- 6. Speed--The important characteristic of a robot that

determines how fast the robot performs the programmed operations.

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CHAPTER II

LITERATURE REVIEW

Introduction

In the early 1960s, the first industrial robot was built under the cooperation of the George Devol and the Unimation company. Since then, industrial robots have been under serious development. Robots are invading the traditional manufacturing system. Totally automated factories are being built and are changing the landscape of manufacturing. In the last few years, the larger industries of the world have invested heavily in robots and automated manufacturing systems. The entrance of many and many companies into the robot business indicates that robotics will be fully implemented in the factories of the future (Heath, 1985; Hunt, 1990).

A robot is a machine that can easily be directed to do a variety of tasks without human supervision. Typical industrial robots are stationary machines, usually bolted to the floor or in an overhead position that can pick up parts and move them about. The basic

concept is to build a machine that is flexible enough to do a variety of jobs automatically, a device that could be easily taught or programmed so that, if the part or process changed, the robot could adapt to its new job without expensive retooling (Health, 1985; Kafrissen, 1984).

Definition

"A robot is a reprogrammable and multifunctional manipulator designed to move materials, parts, tools or specialized devices through various programmable motions in the performance of a variety of tasks" (McDonald, 1986, p. 5). The main applications of industrial robots are:

- * Loading and unloading machine tools;
- * Handling in manufacturing process, such as die casting;
- * Welding;
- * Spray painting;
- * Assembly;
- * Machining, such as deburring and drilling;
- * Inspection. (Koren, 1985, p. 175)

Classification and Types of Robots

Since robot configurations vary greatly, some

classification of robot geometries is necessary. The industry has settled upon the term "degrees of freedom" to describe the number of ways a robot can move. The form of these movements and the way they are assembled make up the robot configuration. Theoretically, there could be a large number of configurations for a robot. From a practical standpoint, however, almost all robots fall into a few popular configuration categories: articulating configurations, polar configurations, cylindrical configurations and cartesian configurations.

The most distinguishing feature used to describe an industrial robot is its power source. The power source usually determines the range of the robot's performance characteristics and in turn the feasibility of various applications. Basically, there are four principal power sources: hydraulic, pneumatic, electric and mechanical gear and cam. Electric robots are popular for precision jobs because they can be closely controlled and can be taught to follow complicated paths of motion. Electric robots can be divided into groups according to the types of electric motors that drive each of the axes of motion. One type uses

stepper motors, which are driven a precise angular displacement for every discrete voltage pulse issued by the control computer interface. The stepper-motor type robot is sometimes of the open-loop type. The other species of electric robot is the dc servo-driven type. These robots invariably incorporate feedback loops from the driven components back to the driver. Thus, the control system continuously monitors the positions of the robot components, compares these positions with the positions desired by the controller, and notes any differences or error conditions.

Another distinguishing feature of the robot is the degree of control possible over the robot motion. This control is affected by the choice of robot drives. Starting from the least sophisticated, we can classify four types of motion control: axis limit, point-topoint, contouring and line tracking. The most complex of contouring motion is line tracking which performs an operation while following alongside a continuously moving path. Line tracking has obvious advantages. The product being processed can be transported on a continuous conveyor instead of an intermittent one.

Although a modern industrial robot looks as though

it is a self-contained, intelligent machine, it is, in fact, a sophisticated combination of many engineering disciplines. The clever interfacing of the various parts has achieved the creation of a powerful tool to serve the pursuit of increased productivity and higher quality of manufactured goods (McDonald, 1986; Asfahl,1985).

In order to design robot systems, a company needs a wide variety of skills. When robots were first designed, mechanical engineering skills were the primary requirement. As robots became part of industrial production, manufacturing engineering skills were needed. As servo control and advanced sensors began to be used, the need for electronics engineers to enter the field became important. Further steps required the skills of programmers, computer hardware engineers, language designers, and vision specialists. The next generation of robots will require people skilled in artificial intelligence and such specialized areas as laser technology and ultrasonics (Poole, 1989).

Significance of the Specifications Generally, industrial robots are built of three

basic systems:

- 1. The mechanical structure consisting of mechanical linkage and joints capable of various movements.
- The control system, which can be of "non-serve" or "serve" type.
- 3. The power units, which can be hydraulic, pneumatic, electrical, mechanical or their combinations.

The variability of these systems' functions and the need for programmability make it a challenge to define a unique set of specifications that engineers can comfortably consider adequate for the final design of robots (Rivin, 1988). Stonecipher (1989) said, "The performance functions that can be analyzed in regard to the actuator are its dynamic capabilities, stability, spatial resolution, control accuracy, repeatability, and compliance" (p. 11).

The most obvious specification determined by the use of a manipulator is the physical or fundamental specification, and Andeen (1988) listed them as follow:

* Payload (Maximum) * Precision absolute accuracy, ability to go to any specified point; repeatability, ability to repeat a location; resolution, the smallest position step; * Speed velocity of the endpoint; cycle time, includes accelerations and decelerations. * Reach

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* Stiffness. (p. 2)
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These specifications are not a set of unrelated numbers, and they may be interrelated. Speed and weight, speed and precision or precision and reach will affect each other. Different payloads in the same speed should not be expected to get the same precision. The designer must recognize that in several performance areas strengthening one specification can decrease performance in another. Resolution, repeatability, and accuracy are the three most important characteristics in evaluating how well an arm can position its end effector (Atkeson, 1986; Andeen, 1988).

Parametric Factors

Robot parameters include kinematic parameters and dynamic parameters. In robotics, the solution of the direct kinematic problem involves the determination of the end effector's position and orientation and their rate of change, as a function of the given positions and speeds of the axes of motion. The position of the end effector, or robot tool, is defined as the TCP (tool center point), which is, for example, the edge of a welding gun or the center of a gripped object.

The kinematic analysis of a mechanical system means the determination of the position, velocity, and acceleration of the various mechanical elements forming the mechanism under consideration. The effect of the associated forces and torques, which take into account the mass and inertia of the mechanical elements, is considered in dynamic analysis (Hollerbach, 1982; N-Nagy, 1987).

In contrast to robot dynamics, one must also consider static conditions. Statics is concerned with forces that act on a body and the conditions required to obtain their equilibrium. Robots require hydraulic, pneumatic, or electric forces to change the position of the free end of the arm. These forces are needed because the robot is a mechanical device that offers resistance to change due to inertia and friction. Once a new position is obtained, the equilibrium has to be reestablished. In this relationship between acting forces and their opposing factors, errors in the response of the robot are produced that must be recognized.

Dynamics also deals with these forces, but it does so with respect to the motion they produce. It

establishes the relationship between acceleration (or deceleration) and the forces involved (Holzbock, 1986).

The robot here is nothing but a transducer changing one form of input into some other form of output. The degree to which the output changes in response to changes in input depends on the accuracy of the robot. When the input calls for a certain position, the robot must act to produce this position. The input is the true value and actual result is the inaccuracy or error. There are dynamic and static errors (Holzbock, 1986).

Static Errors

Holzbock (1986) stated:

Accuracy specifications as given by robot manufacturers practically always refer to the robot arm without end effector and without load being carried. Generally, either one diminishes the specified accuracy. Position accuracy also depends on the deceleration of the motion of the robot arm. For maximum accuracy, the robot has to make final approach to its programmed position very slowly. (p. 3)

But if this high accuracy level is used in program steps where it is not required, cycle time for these steps will be unnecessarily long. This is of particular importance where the motion from one point to another is composed of several steps, for example, when the robot moves around obstacles.

Backlash between two gears that are part of a power transmission produces a dead zone in which no output is produced while the input changes. The increase of the input must first be sufficient to lock the gears together before the output gear begin to follow the input gear. Static friction, also called stiction and break-loose force, is defined as the force required to initiate sliding or rolling motion between two contacting bodies (Holzbock, 1986).

Dynamic Errors

Robot joints are rotational and translational or linear elements that provide elbow, wrist, and other movements. Each degree of freedom of the robot requires its own joint to produce the desired motion. The joints are either directly or remotely driven by actuators that convert electrical, hydraulic, or pneumatic energy into motion.

Mass is a measure of inertia. It is considered a property of matter that resists change of motion. Inertia is the inherent property of bodies to resist any change in their state.

A body in motion may encounter two types of

friction: coulomb friction and viscous friction. Static friction resists the onset of motion, not motion once it takes place. Coulomb friction is also called dry friction or sliding friction. It is caused by minute irregularities of one surface engaging those of the surface over which it slides. It is diminished by lubrication. In a dynamic system, oscillation is generally associated with viscous friction and, hence, is proportional to speed. Oscillation is essential to prevent a system from instability that could otherwise produce excessive oscillations of the end effector of a robot (Holzbock, 1986).

Analysis of Repeatability

Repeatability is the function whereby the robot manipulator is able to repeat or reposition itself into a position that was previously trained or commanded. The internal factors that influence the repeatability of the manipulator system are its movement control system and mechanical components of the robot system (Mason, 1985).

Repeatability is different than accuracy. While accuracy deals with actual spatial position attained by the robot, repeatability deals with positional

discrepancies from cycle to cycle. When comparing repeatability and accuracy, the factors used to determine repeatability will always be of a greater value than absolute accuracy (Stonecipher, 1989; Day, 1988).

Repeatability is sub-classified by Day (1988) into omnidirectional repeatability and unidirectional repeatability. He said, "Repeatability is a function of many variables such as the number of cycles, location in workspace, temperature, speed/acceleration of path, payload, and so forth" (p. 2). So far, there is no unified method of measuring repeatability. Japan Industrial Standards (JIS) uses a seven-cycle measurement. Large robot users, such as General Motors and Ford, have defined their own test procedures to measure repeatability. Other methods of test and specification, such as the use of measurement cubes and spheres have been proposed (Day, 1988).

Environmental factors can also cause inaccuracies and irrepeatability. For example, temperature variations can cause link length changes in structural components and drive-train components. Temperature and relative humidity can affect characteristics of

lubricants used in drive trains (Day, 1988).

Angularity between each pair of adjacent axles also contributes to the inaccuracy of robots. Angularity can come from assembly error of fitting subassemblies together or in the seating of bearings supporting the axles. Day (1988) found, "Just an error of 0.1 degree in angularity could cause a link offset error of 1.745mm when the two adjacent axles were 1000mm apart" (p. 3). Robot accuracy measurement is the first step in understanding what errors are to be corrected.

As Day (1988) suggested, "It is important for users of robots to understand factors affecting [repeatability] and where present technology stands in making [repeatability] improvement" (p. 9).

There are intrinsic limitations in robot manipulators and in robot applications. "It will require joint efforts from users, manipulators, and researchers to achieve the most productive use of [an] accurate robot system" (Day, 1988, p. 9).

CHAPTER III

RESEARCH DESIGN AND METHODOLOGY

Identification of Variables

In this research, there were two independent variables -- payload and speed, and one dependent variable -- repeatability. There were many other variables, such as temperature, humidity, researcher's operating skill, and measurement error, as well as the elastic variation of the robot arm when the payload held by the robot touched the sensor of the dialindicators, all of which could have impacted the repeatability. But during the research process, the researcher mainly aimed at the relative position deviation caused by different working cycles, and not the absolute accuracy of the position an object needs The test was set up in an intensive short to reach. period of time to eliminate environmental effects on repeatability. Therefore, the variables caused by the system might not be considered. Also, the entire study was conducted on the same robot, so other influences caused by the equipment might be omitted.

Instrumentation

The robot program was made with teach pendant, and stored on a 5 1/4" floppy disc. The same program was used repeatedly with different variables (see Appendix A). Cube-shaped plastic and steel blocks were used to exert different payloads. Three dial-indicators were set together to measure the position deviation on X,Y,Z axis separately. Resolution of the dial-indicators is .001 inches.

The payload was held by the gripper with a pressure about 2.5 lbs and also made more tight by the tape around the payload and gripper. During the first few tests, because the measuring set-up did not match with payload well, the reading might not have been accurate. After the researcher changed the shape of some payloads and adjusted the measuring devices, the experiment began to be in process, and went on smoothly.

The gripper always held a certain payload during the 30 cycles. When the robot finished its one cycle and went back to its home position at which the measuring was carried out, there was a 12 second pause for the researcher to read the data, then the robot

automatically went on to the next cycle. The reading was taken as the payload touched the dial-indicators and gave pressure.

The researcher found that after the robot worked for about two to three hours, the heat from the motor made the base part of the robot hot, so when the robot finished one set of 30-cycles, the power of the robot was cut off for about 30-60 minutes to avoid the temperature possibly affecting the results. Before the robot began its first cycle for each pair of payload and speed, all the dial-indicators were set to zero, and the program was set to a new home position, i.e., only the "0" step was changed on a computer. But during the initial setting, human action on equipment might affect the reading of the first cycle, so when the researcher analyzed the data, he considered the position of the first cycle as the "0" position, i.e., the spatial coordinator (X1, Y1, Z1) was considered to be (0,0,0).

Speed/Payload Matrix--Variables Groups

According to the specifications of the MTMR (see appendix B), the payload should range between 0 and 455gm. The maximum number of program steps is 53.

Three maximum non-slip motor speeds correspond to three payloads as shown in Table 1 "Non-slip Motor Speeds vs. Payloads".

TABLE 1: Non-slip Motor Speeds vs. Payloads

| Load | Half-steps per second | Equivalent teach control speed No. |
|-------|--------------------------|---------------------------------------|
| 0 | 400 | 8 |
| 226gm | 206 | 5 |
| 455gm | 99 | 3 |

Therefore, the payload and the speed were set for this experimental research as follows:

TABLE 2: Payloads and Speeds

| payload | 2 | 20gm | 65gm | 130gm | 180gm | 250gm |
|---------|-------|-------|-------|-------|-------|-------|
| speeds | 3,5,7 | 3,5,7 | 3,5,7 | 3,5,7 | 3,5,- | 3,-,- |

<u>Note</u>: For the payload 180gm, speed 7 was not used, in case Motor slip affected results. For the same reason, payload 250gm used speed 3 only.

Data Collection Procedure

The research data of this study were collected during a week of intensive tests. The whole experiment was divided into several groups for analysis. Each group contained one payload with three different speeds. Each pair of payload and speed, such as, 20gm of payload and a speed of 5, was tested during continuous 30 program cycles. Each program cycle gave one reading of position deviation with (@x, @y, @z) coordinates in which @x,@y,@z meant relative axle distance between current position and the original position. Then the relative space distance @D (see Figure 1) was calculated with the following formula:

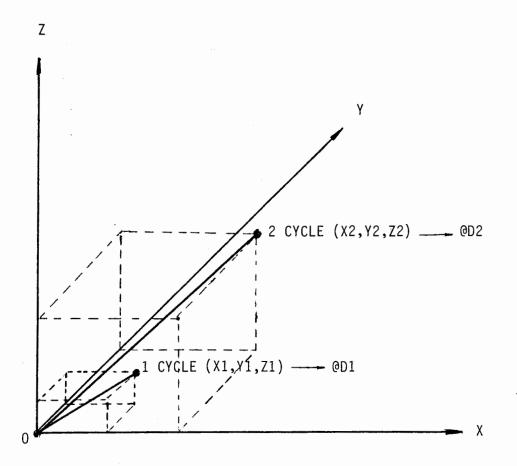
 $QD=SQRT((QX)^{2}+(QY)^{2}+(QZ)^{2})$ <1>

Data Analysis Procedure

In order to analyze the affect of speeds and payloads on repeatability, the mean of the spatial position deviation "@D" and the range of spatial position "R" in 30 cycles was calculated.

@D=(@D1+@D2+...+@D30)/30 <2>

R=@Dmaximum-@Dminimum <3>



Coordinator: O (X0,Y0,Z0); 1 (X1,Y1,Z1); 2 (X2,Y2,Z2).

 $QD1 = SQRT((X1 - X0)^{2} + (Y1 - Y0)^{2} + (Z1 - Z0)^{2})$

 $QD2 = SQRT((X2 - X0)^{2} + (Y2 - Y0)^{2} + (Z2 - Z0)^{2})$

Figure 1: Calculation Demonstration of "QD"

The researcher also developed a linear trend line with a precise statistical method in order to analyze repeatability change in 30 cycles. The "least squares method" was applied here. This approach results in a straight line that minimizes the sum of the squares of the vertical differences from the line to each of the actual observations. The line is expressed as follows:

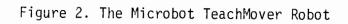
Y*=a+bX* <4>

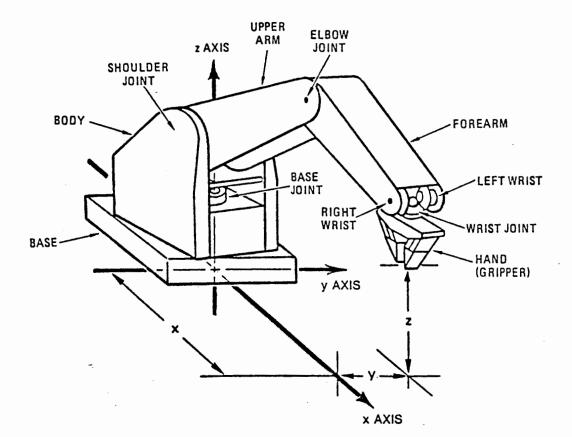
- Note: X*, Y* axis in formula <2> have different meaning from X,Y axis in formula <1>. X,Y,Z coordinates are used as a real position of an object robot handling (see Figure 2), but X*,Y* are used for statistical analysis.

The slope "b" is found by the formula:

 $b = (\sum X * Y * - n\overline{X} * \overline{Y} *) / (\sum X^{2} - n\overline{X}^{2}) \qquad \langle 5 \rangle$

where b=slope of the regression line. ∑=summation sign. X*=the number of program cycles. Y*=computed value of space position deviation "@D".





 \overline{X}^* =the average of the value of the X*. Y*=the average of the value of the Y*. n=the number of data points or observations.

"a" was computed as follows:

a=Y*-bX* <6>

In addition to linear trend line, the coefficient of correlation "r" was calculated with the following equation:

$$r = (n \sum X * Y * - \sum X * \sum Y *) / (n \sum X * - (\sum X *)^{2}) (n \sum Y * - (\sum Y *)^{2}) < 7>$$

$$(-1 < r < 1)$$

A computer program could handle the above calculation "b" and "r'. A microcomputer software package, called AB:POM developed by Howard Weiss, Temple University, was used (see Appendix C). Slope of the regression line "b" and correlation coefficient "r" were used to analyze the distribution of spatial position deviations.

Extended Trend Study of @D

Due to the limitation of time and facility for this research, the researcher used 30 cycles of the program to observe the repeatability and its changing rate. In order to determine if the repeatability

pattern changes beyond 30 cycles, the researcher chose two pairs of speed and payload to execute this task; payload 65 with speed 5 and payload 65 with speed 7. Observations were recorded over 50 cycles under the same program used in the 30 cycles procedure. Spatial deviation @D was calculated the same way.

Robot Program Description

The robot program used in this experiment comprised some basic movements: base rotation, shoulder up-and-down, elbow up-and-down, wrist roll rotation and pitch up-and-down. It included the following steps corresponding to the steps in Appendix A.

<u>STEP</u>

DESCRIPTION

| 0 | Home position. The base at 0 degree position, and shoulder and elbow fully extended with object held in gripper. |
|----|--|
| 1 | Pause 12 seconds, allow researcher to pick up readings between cycles. |
| 2 | Set speeds at 3, 5 or 7. |
| 3 | Raise shoulder and elbow away from home position. |
| 4 | Lower shoulder and elbow. |
| 5 | Rotate base +90 degree. |
| 6 | Raise elbow and shoulder to half-position. |
| 7 | Rotate base -180 degree. |
| 8 | Raise elbow and shoulder, and rise pitch up to limit position. |
| 9 | Rotate base +90 degree to 0 position. |
| 10 | Lower elbow, shoulder, and pitch. |
| 11 | Rotate pitch +90 degree. |
| 12 | Rotate pitch -180 degree. |

- 13 Rotate pitch +90 degree.
- Rotate base +90 degree. 14
- Raise elbow and shoulder. 15
- Rotate base -180 degree. 16
- Lower elbow and shoulder. 17
- Rotate pitch +90 degree. Rotate pitch -90 degree. 18
- 19

-

- Rotate base back to 0 position. 20
- Raise shoulder and elbow, and raise pitch up 21 above home position.
- Smoothly lower shoulder and elbow to reach 22 home position and touch the dial-indicator.

CHAPTER IV

PRESENTATION AND ANALYSIS OF DATA

Results of Experiment

Following the procedures set in the methodology, the researcher finished testing fifteen pairs of payloads and speeds under thirty cycles and two pairs of payloads and speeds under fifty cycles. All the data are shown on the tables from Table 3 to Table 19, which include payload 65g and speed 5 as well as payload 65g and speed 7 with fifty cycles.

Each table contains the results of only one pair of payload and speed. @X, @Y, @Z were calculated with formulas: @X = X-X1, @Y = Y-Y1 and @Z = Z-Z1, in which (X1, Y1, Z1) is the coordinate of the first cycle's position. Because at the beginning of test, even though the researcher set the three dial-indicators at 0 positions, human action on equipment might affect the reading of the first cycles. Therefore the first cycle's position was considered as "0" position, then the other cycles' deviation @X, @Y, @Z can be looked as the relative distance from the first cycle's position.

As the researcher mentioned before, in this research, relative deviation is more significant than absolute deviation, because the repeatability is only concerned about position change cycle by cycle. Spatial deviation @D were calculated based on @X, @Yand @Z, i.e., @D= SQRT ($\text{@X}^2+\text{@Y}^2+\text{@Z}^2$). The mean spatial deviation @D and the range of deviation R during the thirty cycles were calculated and the results shown in Table 3 to Table 17. Table 18 and Table 19 would be used for the trend analysis of deviation changes. The unit used for the deviation in these tables are .001 inches. And the symbol "+" (omitted in tables) and "-" can be referenced to the Figure 2. For example, "@Z= -1.5" means the direction of position change is downward on Z axis.

From these tables, it can be seen that both payload and speed had an effect on the position deviation, i.e., the repeatability. Especially the payload from 0 to 130gm could satisfactorily indicate how they affected the repeatability. The heavy payload such as 180g and 250g sometimes made the robot motor slip during the test, which could affect the accuracy of the results.

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Spatial Deviation for Payload (2) and Speed (3)

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Spatial Deviation (in .001 inches)

| - | | | | | |
|-------|------|-----|------|------------------------|--|
| Cycle | @x | @y | @z | +@SQRT(@x^2+@y^2+@z^2) | |
| 1 | 0 | 0 | 0 | 0 | |
| 2 | 1.4 | 0 | 6.9 | 7.0405 | |
| 3 | 7.2 | 0.1 | 7.5 | 10.397 | |
| 4 | 5.6 | 0.3 | 8.8 | 10.435 | |
| 5 | 7.2 | 0.9 | 9.7 | 12.113 | |
| 6 | 8.8 | 0.9 | 9.8 | 13.201 | |
| 7 | 10.1 | 1 | 12.8 | 16.335 | |
| 8 | 11.4 | 1.1 | 15.6 | 19.352 | |
| 9 | 12.8 | 1.2 | 16.6 | 20.996 | |
| 10 | 13.7 | 1.2 | 18.8 | 23.293 | |
| 11 | 14.7 | 1.5 | 21.7 | 26.253 | |
| 12 | 15.7 | 1.9 | 26.9 | 31.204 | |
| 13 | 13.8 | 1.9 | 18.7 | 23.318 | |
| 14 | 15.8 | 2 | 29.9 | 33.876 | |
| 15 | 17.8 | 1.9 | 31.5 | 36.231 | |
| 16 | 18.7 | 1.8 | 32.9 | 37.885 | |
| 17 | 19.5 | 2 | 34.7 | 39.853 | |
| 18 | 20.1 | 1.8 | 37.5 | 42.585 | |
| 19 | 20.8 | 1.7 | 36.7 | 42.218 | |
| 20 | 21.3 | 1.8 | 36.8 | 42.557 | |
| 21 | 21.8 | 2 | 41.8 | 47.185 | |
| 22 | 22.5 | 2 | 42.7 | 48.306 | |
| 23 | 23 | 1.8 | 44.7 | 50.302 | |
| 24 | 23.4 | 2 | 46.8 | 52.362 | |
| 25 | 23.9 | 1.7 | 47.9 | 53.558 | |
| 26- | 24.5 | 1.5 | 48.2 | 54.090 | |
| 27 | 24.9 | 1.1 | 49.7 | 55.599 | |
| 28 | 25.2 | 1.1 | 49.8 | 55.823 | |
| 29 | 25.5 | 1.1 | 53.2 | 59.005 | |
| 30 | 26 | 1.2 | 52.2 | 58.329 | |

Note. @D=(@D1+@D2+...+@D30)/30=42.08 R=@Dmax-@Dmin=59

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Spatial Deviation for Payload (2) and Speed (5)

....

Spatial Deviation (in .001 inches)

| Cycl | @x | @y | @z | +@SQRT(@x^2+@y^2+@z^ 2) |
|------|------|------|------|-------------------------|
| 1 | 0 | 0 | 0 | 0 |
| 2 | 0.8 | 2.8 | 2.4 | 3.7735 |
| 3 | 1.7 | 5.9 | 3.5 | 7.0675 |
| 4 | 2.6 | 8.9 | 3.8 | 10.020 |
| 5 | 3.6 | 11.6 | 4.8 | 13.059 |
| 6 | 4.5 | 12.6 | 5.9 | 14.622 |
| 7 | 5.5 | 13.9 | 6.8 | 16.422 |
| 8 | 5.9 | 15 | 6.9 | 17.533 |
| 9 | 6.9 | 16 | 8 | 19.173 |
| 10 | 7.1 | 16.8 | 8.6 | 20.164 |
| 11 · | 7.4 | 17.8 | 12 | 22.706 |
| 12 | 8 | 18.9 | 10 | 22.830 |
| 13 | 8.4 | 19.8 | 9.9 | 23.677 |
| 14 | 8.9 | 21.8 | 12 | 26.428 |
| 15 | 9.4 | 22.4 | 12.8 | 27.458 |
| 16 | 9.6 | 22.6 | 14.6 | 28.567 |
| 17 | 10.4 | 22.6 | 16.2 | 29.687 |
| 18 | 10.5 | 22.9 | 15.5 | 29.578 |
| 19 | 10.9 | 23.8 | 17 | 31.212 |
| 20 | 11.4 | 24.2 | 17.2 | 31.803 |
| 21 | 11.6 | 24.1 | 18.8 | 32.692 |
| 22 | 12 | 24.7 | 18.5 | 33.111 |
| 23 | 12.4 | 24.3 | 20 | 33.826 |
| 24 | 12.7 | 24.8 | 20.9 | 34.830 |
| 25 | 12.9 | 25.4 | 22 | 35.994 |
| 26- | 13.5 | 25.8 | 23 | 37.106 |
| 27 | 13.8 | 25.7 | 23 | 37.147 |
| 28 | 13.9 | 25.7 | 24.2 | 37.938 |
| 29 | 14.2 | 25.4 | 24.1 | 37.783 |
| 30 | 14.7 | 25.4 | 25 | 38.551 |

Note. @D=(@D1+@D2+...+@D30)/30=25.16 R=@Dmax-@Dmin=38.55

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Spatial Deviation for Payload (2) and Speed (7)

Spatial Deviation (in .001 inches)

| - | | | | |
|-------|-----|------|------|-----------------------|
| Cycle | @x | @y | @z | @SQRT(@x^2+@y^2+@z^2) |
| 1 | 0 | | 0 | 0 |
| 2 | 1 | 2.9 | -0.7 | 3.1464 |
| 3 | 1.3 | 6.2 | 4.2 | 7.6006 |
| 4 | 1.7 | 8 | -0.2 | 8.1810 |
| 5 | 1.9 | 11.6 | -1.6 | 11.862 |
| 6 | 2.1 | 14.1 | -1.7 | 14.356 |
| 7 | 2.5 | 15.3 | -3.2 | 15.829 |
| 8 | 2.6 | 18.3 | -3.3 | 18.776 |
| 9 | 2.8 | 20.1 | -3.9 | 20.665 |
| 10 | 3.4 | 22.1 | -5.6 | 23.050 |
| 11 | 3.5 | 24 | -5.6 | 24.891 |
| 12 | 3.7 | 27 | -5.9 | 27.883 |
| 13 | 3.8 | 29.1 | -5 | 29.769 |
| 14 | 4.2 | 30.5 | -5.7 | 31.311 |
| 15 | 4.3 | 32.1 | -5.7 | 32.884 |
| 16 | 4.7 | 33.6 | -5.8 | 34.419 |
| 17 | 5 | 34.3 | -5.8 | 35.144 |
| 18 | 5.4 | 34.6 | -4.8 | 35.346 |
| 19 | 5.8 | 35.1 | -4.8 | 35.898 |
| 20 | 5.8 | 38.6 | -4.8 | 39.327 |
| 21 | 6.1 | 39.9 | -4 | 40.561 |
| 22 | 6.5 | 39.1 | -3.9 | 39.828 |
| 23 | 6.9 | 39.9 | -4.2 | 40.709 |
| 24 | 7.1 | 40 | -4 | 40.821 |
| 25 | 7.5 | 40.6 | -3.7 | 41.452 |
| 26- | 8 | 41.9 | -4 | 42.844 |
| 27 | 8.3 | 42.2 | -2.3 | 43.069 |
| 28 | 8.3 | 43.1 | -2.3 | 43.952 |
| 29 | 8.4 | 44.2 | -2.2 | 45.044 |
| 30 | 8.8 | 44.9 | -0.9 | 45.763 |

Note. @D=(@D1+@D2+...+@d30)/30=29.15 R=@Dmax-@Dmin=45.76

.

Spatial Deviation for Payload (20) and Speed (3)

Spatial Deviation (in .001 inches)

| - | | | | |
|-------|------|------|-------|-----------------------|
| Cycle | @x | @y | @z | @SQRT(@x^2+@y^2+@z^2) |
| | 0 | 0 | 0 | 0 |
| 2 | 3.1 | 1.5 | 6 | 6.9180 |
| 3 | 5.3 | 3 | 11.5 | 13.013 |
| 4 | 5.5 | 3.9 | 10.1 | 12.143 |
| 5 | 7.5 | 4.3 | 19.9 | 21.696 |
| 6 | 10.2 | 5.6 | 27.6 | 29.952 |
| 7 | 12.7 | 6.2 | 36.6 | 39.233 |
| 8 | 18 | 7.4 | 56 | 59.285 |
| 9 | 19.8 | 8.3 | 60.3 | 64.007 |
| 10 | 22.2 | 9.1 | 66.1 | 70.319 |
| 11 | 24.7 | 9.3 | 72.7 | 77.342 |
| 12 | 25 | 10.1 | 70.9 | 75.853 |
| 13 | 26.7 | 11.2 | 75.5 | 80.861 |
| 14 | 28.2 | 11.3 | 82.7 | 88.103 |
| 15 | 29.9 | 11.6 | 88.1 | 93.755 |
| 16 | 30.5 | 11.5 | 94.5 | 99.963 |
| 17 | 32.9 | 11.2 | 101.3 | 107.09 |
| 18 | 34.3 | 11.1 | 105.1 | 111.11 |
| 19 | 35.3 | 11.7 | 111.1 | 117.15 |
| 20 | 36.3 | 11.1 | 113.6 | 119.77 |
| 21 | 38 | 12 | 121.3 | 127.67 |
| 22 | 39.7 | 11.2 | 124.5 | 131.15 |
| 23 | 40.3 | 11.3 | 130.3 | 136.85 |
| 24 | 41.5 | 12.1 | 134.6 | 141.37 |
| 25 | 42.7 | 12 | 144 | 150.67 |
| 26- | 43.6 | 11.2 | 144.6 | 151.44 |
| 27 | 44.4 | 12.1 | 147.3 | 154.32 |
| 28 | 45.5 | 12.9 | 150.7 | 157.94 |
| 29 | 46.4 | 13 | 154 | 161.36 |
| 30 | 47.3 | 13 | 157 | 164.48 |
| | | | | |

Note. @D=(@D1+@D2+...+@D30)/30=92.16 R=@Dmax-@Dmin=164.48

.

Spatial Deviation for Payload (20) and Speed (5)

Spatial Deviation (in .001 inches)

| Cycle | @x | @y | @z | @SQRT(@x^2+@y^2+@z^2) |
|-----------------|------|--------------|------|-----------------------|
| 1 | 0 | 0 | 0 | 0 |
| 2 | 0.6 | 2.1 | 0.2 | 2.1931 |
| 3 | 1.4 | 9 | 2.5 | 9.4451 |
| 4 | 2.2 | 13.8 | 3.6 | 14.430 |
| 5 | 2.9 | 15.1 | 4.5 | 16.020 |
| 6 | 3.7 | 13.8 | 4.8 | 15.072 |
| 7 | 4.9 | 14.5 | 2.5 | 15.508 |
| 8 | 5.4 | 17.7 | 4 | 18.932 |
| 9 | 6.2 | 18.8 | 5.4 | 20.519 |
| 10 | 7.1 | 24 | 8.4 | 26.400 |
| 11 | 7.7 | 21.9 | 9 | 24.897 |
| 12 | 8.6 | 26.6 | 11 | 30.041 |
| 13 | 9.2 | 24.5 | 12.5 | 29.002 |
| 14 | 9.9 | 25 | 13.8 | 30.223 |
| 15 | 9.6 | 24.2 | 15.5 | 30.299 |
| 16 | 11.2 | 24.9 | 18.5 | 32.980 |
| 17 | 11.6 | 26.5 | 19.8 | 35.054 |
| 18 | 11.8 | 26.9 | 20.4 | 35.763 |
| 19 | 12.6 | 27.1 | 21.2 | 36.641 |
| 20 | 13.9 | 26.9 | 23.1 | 38.084 |
| 21 | 13.2 | 27.7 | 24.7 | 39.390 |
| 22 | 13.9 | 27.9 | 28.1 | 41.967 |
| 23 | 14.5 | 27 .9 | 28.9 | 42.706 |
| 24 | 14.9 | 28 | 32.7 | 45.555 |
| 25 | 15.4 | 31.1 | 33.5 | 48.235 |
| 26 ⁻ | 16.8 | 29.2 | 35.6 | 49.012 |
| 27 | 16.4 | 29.4 | 35.7 | 49.069 |
| 28 | 16.8 | 29 | 37.1 | 49.996 |
| 29 | 17.1 | 28.5 | 37.7 | 50.258 |
| 30 | 17.5 | 29.9 | 38.5 | 51.792 |

Note. @D=(@D1+@D2+...+@D30)/30=30.98 R=@Dmax-@Dmin=51.79

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Spatialeviatiofor Payload (20) and Speed (7)

Spatialeviation (in .001 inches)

| Cycle | @x | @y | @z | @SQRT(@x^2+@y^2+@y^2) |
|-------|-------|------|-------|------------------------|
| 1 | 0 | 0 | | 0 |
| 2 | -0.8 | 3.7 | 2.4 | 4.4821 |
| 3 | -1.8 | 6.3 | -2.2 | 6.9115 |
| 4 | -2.9 | 9.7 | -6.9 | 12.251 |
| 5 | -2.8 | 13.9 | -6.9 | 15.768 |
| 6 | -1.9 | 18 | -10.1 | 20.727 |
| 7 | -2.8 | 22.6 | -13.3 | 26.372 |
| 8 | -2.5 | 25.9 | -14.7 | 29.885 |
| 9 | -1.7 | 29.6 | -15.2 | 33.318 |
| 10 | -1.3 | 33.3 | -17 | 37.410 |
| 11 | -0.6 | 36.5 | -18 | 40.701 |
| 12 | 0.3 | 38.3 | -17 | 41.904 |
| 13 | 0.7 | 41.6 | -17.9 | 45.293 |
| 14 | 1.7 | 46.5 | -18 | 49.891 |
| 15 | 2.7 | 47.5 | -17.2 | 50.590 |
| 16 | 3.9 | 50.5 | -15 | 52.824 |
| 17 | 4.9 | 52.1 | -15.1 | 54.464 |
| 18 | 5.2 | 53.6 | -13.4 | 55.493 |
| 19 | 6.5 | 54.9 | -9.6 | 56.110 |
| 20 | - 6.9 | 57.4 | -8.9 | 58.494 |
| 21 | 7.5 | 57.4 | -6.7 | 58.274 |
| 22 | 8.5 | 58.8 | -5.3 | 59.647 |
| 23 | 9.2 | 63.4 | -5 | 64.258 |
| 24 | 10 | 62.6 | -3.6 | 63.495 |
| 25 | 10.8 | 62.6 | -3.6 | 63.626 |
| 26- | 11.2 | 63.9 | -0.1 | 64.874 |
| 27 | 11.7 | 64.5 | 0.1 | 65.552 |
| 28 | 12.3 | 65.6 | 0.9 | 66.749 |
| 29 | 12.7 | 66.6 | 2.4 | 67.842 |
| 30 | 13.2 | 67.5 | 4.1 | 68.900 |

Note. @D=(@D1+@D2+...+@D30)/30=44.54 R=@Dmax-@Dmin=68.9

,

Spatial Deviation for Payload (65) and Speed (3)

Spatial Deviation (in .001 inches)

| Cycle | @x | @y | @z | @SQRT(@x^2+@y^2+@z^2) |
|-----------------|------|------|-------|-----------------------|
| 1 | 0 | 0 | 0 | 0 |
| 2 | 2.6 | -0.1 | 17.7 | 17.890 |
| 3 | 4.4 | 0.8 | 30.2 | 30.529 |
| 4 | 7.2 | 1.8 | 38.4 | 39.110 |
| 5 | 9.2 | 2.4 | 46.2 | 47.168 |
| 6 | 11 | 3.7 | 53.7 | 54.939 |
| 7 | 13 | 3.6 | 0 | 13.489 |
| 8 | 14.9 | 3 | 69.1 | 70.751 |
| 9 | 16.8 | 3.4 | 77.1 | 78.982 |
| 10 | 18.6 | 3.1 | 78.6 | 80.830 |
| 11 | 20 | 2.8 | 91.3 | 93.506 |
| 12 | 21.5 | 2.8 | 98.3 | 100.66 |
| 13 | 22.9 | 2.7 | 105.9 | 108.38 |
| 14 | 24.5 | 2.6 | 112.7 | 115.36 |
| 15 | 25.9 | 1.9 | 119.9 | 122.68 |
| 16 | 26.7 | 2.9 | 127.4 | 130.20 |
| 17 | 27.9 | 2.8 | 130.6 | 133.57 |
| 18 | 29.2 | 3.3 | 136.3 | 139.43 |
| 19 | 30.4 | 3.7 | 142.7 | 145.94 |
| 20 | 31.5 | 2.7 | 146.3 | 149.67 |
| 21 | 32.2 | 2.8 | 148.9 | 152.36 |
| 22 | 33.3 | 3 | 153.8 | 157.39 |
| 23 | 34.3 | 2.7 | 159.7 | 163.36 |
| 24 | 34.8 | 2.8 | 164.3 | 167.96 |
| 25 | 35.6 | 3.2 | 169.1 | 172.83 |
| 26 ⁻ | 36.4 | 2.9 | 171.7 | 175.53 |
| 27 | 37.2 | 3 | 175.9 | 179.81 |
| 28 | 37.8 | 2.8 | 179 | 182.96 |
| 29 | 38.5 | 2.6 | 182.2 | 186.24 |
| 30 | 39.4 | 2.3 | 184.2 | 188.38 |

Note. @D=(@D1+@D2+...+@D30)/30=113.33 R=@Dmax-@Dmin=188.38

.

Spatial Deviation for Payload (65) and Speed (5)

Spatial Deviation 9in .001 inches)

| Cycle | @x | @у | @z | @SQRT(@x^2+@y^2+@z^2) |
|-------|-------|------|------|-----------------------|
| 1 | 0 | 0 | 0 | 0 |
| 2 | 1.2 | 2.2 | 3.1 | 3.9862 |
| 3 | 1.4 | 3.9 | 7.1 | 8.2207 |
| 4 | 1.4 | 5.9 | 10.8 | 12.385 |
| 5 | 1.6 | 8.5 | 14 | 16.456 |
| 6 | 1.8 | 11.5 | 19.3 | 22.538 |
| 7 | 1.9 | 12.1 | 20.8 | 24.138 |
| 8 | 2 | 16.6 | 24.2 | 29.414 |
| 9 | 2 | 18.5 | 25 | 31.164 |
| 10 | 2.1 | 20.1 | 27.4 | 34.046 |
| 11 | 2.4 | 20.5 | 31.2 | 37.409 |
| 12 | 2.5 | 23 | 35.2 | 42.122 |
| 13 | 2.7 | 25.3 | 37.4 | 45.234 |
| 14 | 3 | 27.4 | 42.7 | 50.823 |
| 15 | 3 | 27 | 42.7 | 50.609 |
| 16 | 3.2 | 27.6 | 44.3 | 52.292 |
| 17 | 3.6 | 30.1 | 48.3 | 57.025 |
| 18 | 4 | 30.2 | 51.3 | 59.663 |
| 19 | 4.2 | 31.3 | 51.2 | 60.156 |
| 20 | - 4.4 | 35.3 | 54.3 | 64.914 |
| 21 | 4.8 | 31.6 | 57 | 65.349 |
| 22 | 5 | 33.2 | 60.3 | 69.016 |
| 23 | 5.4 | 33 | 62.1 | 70.530 |
| 24 | 6 | 34 | 64.2 | 72.894 |
| 25 | 6.1 | 34 | 66.3 | 74.758 |
| 26- | 6.1 | 36.5 | 68.3 | 77.681 |
| 27 | 6.3 | 34.4 | 70.4 | 78.607 |
| 28 | 6.9 | 33.7 | 73.6 | 81.241 |
| 29 | 7 | 34 | 75.2 | 82.825 |
| 30 | 7.2 | 39 | 75.5 | 85.282 |

Note. @D=(@D1+@D2+...+@d30)/30=48.72 R=@Dmax-@Dmin=85.28

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Spatial Deviation for Payload (65) and Speed (7)

| Cycle | @x | @у | @z | @SQRT(@x^2+@y^2+@z^2) |
|-------|----------|------|-------|-----------------------|
| 1 | 0 | 0 | | 0 |
| 2 | 3.5 | 2 | 18.4 | 18.836 |
| 3 | 4.9 | 5 | 27.6 | 28.474 |
| 4 | 5.8 | 6.5 | 33.5 | 34.614 |
| 5 | 6.4 | 8.2 | 37.5 | 38.915 |
| 6 | 7 | 9.1 | 40.7 | 42.288 |
| 7 | 7.6 | 10.3 | 44.4 | 46.208 |
| 8 | 8.1 | 10.1 | 48.4 | 50.101 |
| 9 | 8.4 | 11 | 50.9 | 52.748 |
| 10 | 11.5 | 12 | 63 | 65.155 |
| 11 . | 12.5 | 15.3 | 69 | 71.772 |
| 12 | 13.5 | 14.1 | 74.3 | 76.821 |
| 13 | 14.4 | 15.3 | 78.4 | 81.166 |
| 14 | 15.4 | 15.9 | 83.5 | 86.384 |
| 15 | 16.4 | 19.6 | 87.7 | 91.347 |
| 16 | 17.4 | 17.1 | 92.3 | 95.469 |
| 17 | 18 | 17.6 | 94.6 | 97.892 |
| 18 | 18.3 | 21.6 | 98 | 102.00 |
| 19 | 18.5 | 19.9 | 99.3 | 102.95 |
| 20 | <u> </u> | 20 | 101 | 104.69 |
| 21 | 19.1 | 20.5 | 102.6 | 106.35 |
| 22 | 19.4 | 21.2 | 104.4 | 108.28 |
| 23 | 19.7 | 21.6 | 107.2 | 111.11 |
| 24 | 20 | 21.6 | 107.9 | 111.84 |
| 25 | 20.4 | 22 | 108.6 | 112.66 |
| 26- | 20.8 | 22 | 111.5 | 115.53 |
| 27 | 21.3 | 23.6 | 113.6 | 117.96 |
| 28 | 21.3 | 23.8 | 115.7 | 120.02 |
| 29 | 21.8 | 23.6 | 118 | 122.29 |
| 30 | 21.9 | 23.6 | 118.6 | 122.89 |

Spatial Deviation for Payload (65) and Speed (7)

Note. @D=(@D1+@D2+...+@D30)/30=81.23 R=@Dmax-@Dmin=122.89

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spatial Deviation for Payload (130) and Speed (3)

Spatial Deviation (in .001 inches)

| - | | | | | |
|-------|-------|------|------|----------------------|--|
| Cycle | @x | @y | @z | @SQRT(@x^2+@y^2+@z^2 | |
| 1 | 0 | 0 | 0 | 0 | |
| 2 | -3.3 | 7 | -4.6 | 9.0027 | |
| 3 | -2.8 | 11.5 | 1.3 | 11.907 | |
| 4 | -1.9 | 15.2 | 9.2 | 17.868 | |
| 5 | -1.3 | 18.6 | 16.2 | 24.7 | |
| 6 | 0.2 | 20.1 | 25.3 | 32.313 | |
| 7 | 0.9 | 22.4 | 30.2 | 37.611 | |
| 8 | 1.2 | 24.2 | 37.1 | 44.311 | |
| 9 | 1.8 | 25.2 | 43.1 | 49.958 | |
| 10 | 2.2 | 26.1 | 45.5 | 52.500 | |
| 11 | 2.6 | 25.9 | 47.3 | 53.989 | |
| 12 | -1.3 | 27.1 | 33 | 42.721 | |
| 13 | 4.8 | 29 | 59.1 | 66.006 | |
| 14 | 0.3 | 29 | 42.2 | 51.204 | |
| 15 | 4.4 | 31 | 59.1 | 66.881 | |
| 16 | 0.2 | 31.9 | 43.2 | 53.701 | |
| 17 | 0.2 | 30.5 | 43.3 | 52.963 | |
| 18 | 0.1 | 31.1 | 43.1 | 53.149 | |
| 19 | 0.1 | 31.6 | 43 | 53.362 | |
| 20 | - 0.4 | 31.5 | 45.3 | 55.176 | |
| 21 | 4.8 | 32 | 63.1 | 70.912 | |
| 22 | 4.5 | 33.2 | 60.5 | 69.157 | |
| 23 | 4.4 | 32.5 | 60 | 68.378 | |
| 24 | 4.4 | 33.2 | 60.1 | 68.801 | |
| 25 | 3.8 | 33.5 | 60.9 | 69.609 | |
| 26- | 3.8 | 33.2 | 59.2 | 67.980 | |
| 27 | 4.5 | 33 | 61.1 | 69.587 | |
| 28 | 3.8 | 33.1 | 59.7 | 68.367 | |
| 29 | 3.9 | 33.1 | 42.9 | 54.325 | |
| 30 | 4.7 | 33.1 | 43.1 | 54.546 | |

Note. <u>@D</u>=(@D1+@D2+...+@D30)/30=49.67 R=@Dmax-@Dmin=70.91

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Spatial Deviation for Payload (130) and Speed (5)

Spatial Deviation (in .001 inches)

| Cycle | @x | @у | @z | @SQRT(@x^2+@y^2+@z^2) |
|-------|------|------|------|-----------------------|
| 1 | 0 | 0 | 0 | 0 |
| 2 | 5.9 | 4.3 | 16.7 | 18.226 |
| 3 | 8.2 | 9 | 24.7 | 27.537 |
| 4 | 4.5 | 13.3 | 26.7 | 30.166 |
| 5 | -0.3 | 16.9 | 22.8 | 28.382 |
| 6 | -2.5 | 21.5 | 23 | 31.583 |
| 7 | -2.7 | 26.4 | 27.4 | 38.144 |
| 8 | 0.6 | 30.3 | 42.1 | 51.873 |
| 9 | 0.9 | 33.4 | 48.1 | 58.566 |
| 10 | 1.4 | 33.4 | 54 | 63.509 |
| 11 - | 1.2 | 39.6 | 59.5 | 71.483 |
| 12 | 1.7 | 42.4 | 62.5 | 75.544 |
| 13 | 1.5 | 44.6 | 63.6 | 77.694 |
| 14 | 0.2 | 44.6 | 65.4 | 79.160 |
| 15 | 0.1 | 47.6 | 68.6 | 83.496 |
| 16 | -0.1 | 49.6 | 70.5 | 86.199 |
| 17 | -0.3 | 51.5 | 72.5 | 88.930 |
| 18 | -0.3 | 53.4 | 74.6 | 91.743 |
| 19 | -0.5 | 55 | 75.1 | 93.087 |
| 20 | -0.3 | 58.4 | 79 | 98.242 |
| 21 | -0.5 | 57.5 | 79.7 | 98.278 |
| 22 | -0.5 | 58.5 | 81.6 | 100.40 |
| 23 | -0.4 | 58.6 | 82.9 | 101.52 |
| 24 | -0.2 | 59.3 | 85.3 | 103.88 |
| 25 | 0 | 60.5 | 87.5 | 106.37 |
| 26- | -0.2 | 61.4 | 87.5 | 106.89 |
| 27 | 0 | 61.7 | 89.6 | 108.78 |
| 28 | -0.3 | 61.7 | 89.2 | 108.46 |
| 29 | -0.2 | 61.6 | 91.3 | 110.13 |
| 30 | -0.2 | 62.5 | 90.6 | 110.06 |

Note. @D=(@D1+@D2+...+@D30)/30=74.93 R=@Dmax-@Dmin=110.14

Spatial Deviation for payload (130) and Speed (7)

Spatial Deviation (in .001 inches)

 $@SQRT(@x^2+@y^2+@z^2)$ Cycle @z @x @y 0 0 0 1 0 2 0 4.4 1.8 4.7539 5 3 9.4 18.4 21.258 4 6.6 12 27.3 30.542 5 7.7 33.6 37.836 15.6 6 8.6 17.9 40.2 44.837 7 9.2 20.8 44 49.530 8 9.9 22.9 48.7 54.718 9 10.6 27.5 52.7 60.381 10 11.2 30.2 57.3 65.732 11 31.9 64.4 72.895 12.2 12 34.6 80.837 13.5 71.8 13 14.2 37.4 77.3 87.038 14 15.4 39 84.9 94.689 15 16.8 41.4 93.4 103.53 16 17.9 43.9 **99.**7 110.39 17 45.7 116.40 18.8 105.4 18 26.8 47.5 134.3 144.95 19 27 50.3 137.2 148.60 20 27.1 50.4 140.9 152.07 21 27.1 52.5 142.9 154.63 22 27.3 53.9 144.2 156.34 23 27.5 55.3 146.7 159.17 24 27.5 54.4 147.6 159.69 25 27.8 162.15 55.5 149.8 164.97 26-28.1 55.5 152.8 27 28.4 57.4 155.3 167.98 28 28.7 **57.9** 157.1 169.87 29 59.4 28.9 159.3 172.45 30 29.2 60.5 161.5 174.91

Note. @D=(@D1+@D2+...+@D30)/30=104.11 R=@Dmax-@Dmin=174.91

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Spatial Deviation for payload (180) and Speed (3)

Spatial Deviation (in .001 inches)

| Cycle | @x | @y | @z | @SQRT(@x^2+@y^2+@z^2) |
|-------|-------|------|------|------------------------|
| | 0 | 0 | 0 | 0 |
| 2 | 1.5 | 2.9 | 15.6 | 15.938 |
| 3 | 2.1 | 4.3 | 28.6 | 28.997 |
| 4 | 2.9 | 5.4 | 43.1 | 43.533 |
| 5 | 3.2 | 5.4 | 45.4 | 45.831 |
| 6 | 3.4 | 6.1 | 49.6 | 50.089 |
| 7 | 3.2 | 9 | 49.3 | 50.216 |
| 8 | 3.2 | 9.1 | 49.3 | 50.234 |
| 9 | 2.8 | 10.9 | 47.3 | 48.620 |
| 10 | 3.1 | 11.9 | 48.8 | 50.325 |
| 11 | 3.4 | 12.4 | 50.6 | 52.208 |
| 12 | 3.6 | 12.1 | 52.1 | 53.607 |
| 13 | 3.8 | 11.4 | 54.1 | 55.418 |
| 14 | 3.8 | 13.4 | 52.5 | 54.316 |
| 15 | 3.5 | 13.9 | 49.1 | 51.149 |
| 16 | 3.5 | 13.9 | 45.1 | 47.323 |
| 17 | 3.5 | 13.4 | 48.3 | 50.246 |
| 18 | 3.4 | 13.9 | 45.1 | 47.315 |
| 19 | 3.4 | 13.9 | 45.3 | 47.506 |
| 20 | - 3.4 | 14.1 | 46.6 | 48.805 |
| 21 | 3.5 | 13.9 | 45.6 | 47.799 |
| 22 | 3.3 | 13.6 | 46.6 | 48.656 |
| 23 | 3.4 | 14.1 | 45.3 | 47.565 |
| 24 | 3.3 | 15 | 42.2 | 44.908 |
| 25 | 3.1 | 13.8 | 44.1 | 46.312 |
| 26- | 3.2 | 14 | 45.1 | 47.331 |
| 27 | 3 | 14.4 | 41.4 | 43.935 |
| 28 | 3.1 | 15 | 42 | 44.705 |
| 29 | 2.9 | 14.6 | 41.6 | 44.182 |
| 30 | 3 | 14.8 | 38.6 | 41.448 |

Note. <u>@D</u>=(@D1+@D2+...+@D30)/30=44.95 R=@Dmax-@Dmin=55.42

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Spatial Deviation for Payload (180) and Speed (5)

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Spatial Deviation (in .001 inches)

| - | | | | |
|-------|-----|-----|------|-----------------------|
| Cycle | @x | @y | @z | @SQRT(@x^2+@y^2+@z^2) |
| | 0 | 0 | 0 | 0 |
| 2 | 0.2 | 5.8 | 0 | 5.8034 |
| 3 | 0.2 | 3.8 | 3.6 | 5.2383 |
| 4 | 0.2 | 1.3 | -9.4 | 9.4915 |
| 5 | 0.4 | 1.6 | 1.4 | 2.1633 |
| 6 | 0.3 | 1.7 | 0 | 1.7262 |
| 7 | 0.4 | 1.3 | 1.4 | 1.9519 |
| 8 | 0.4 | 6.7 | 0.6 | 6.7386 |
| 9 | 0.5 | 6.9 | 0.4 | 6.9296 |
| 10 | 0.5 | 6.3 | -0.5 | 6.3395 |
| 11 | 0.5 | 3.7 | -0.9 | 3.8405 |
| 12 | 0.3 | 3.3 | -2.3 | 4.0336 |
| 13 | 0.3 | 2.9 | -1.4 | 3.2341 |
| 14 | 0.3 | 3 | -2.3 | 3.7920 |
| 15 | 0.3 | 2.2 | -1.4 | 2.6248 |
| 16 | 0.5 | 2.3 | 1.5 | 2.7910 |
| 17 | 0.4 | 7.3 | -2 | 7.5795 |
| 18 | 0.4 | 3.7 | -0.5 | 3.7549 |
| 19 | 0.3 | 3.8 | 0 | 3.8118 |
| 20 | 0.3 | 3.7 | -0.5 | 3.7456 |
| 21 | 0.6 | 3.6 | 1.3 | 3.8742 |
| 22 | 0.6 | 3.5 | 0.6 | 3.6013 |
| 23 | 0.6 | 7.3 | -1.1 | 7.4067 |
| 24 | 0.4 | 6.7 | -0.6 | 6.7386 |
| 25 | 0.4 | 4.8 | -0.6 | 4.8538 |
| 26- | 0.4 | 4 | 1.4 | 4.2567 |
| 27 | 0.3 | 4.8 | 1.3 | 4.9819 |
| 28 | 0.3 | 4.3 | -0.6 | 4.3520 |
| 29 | 0.3 | 4.7 | -0.5 | 4.7360 |
| 30 | 0.5 | 6.4 | 0.5 | 6.4389 |
| | | | | |

Note. @D=(@D1+@D2+...+@D30)/30=4.56 R=@Dmax-@Dmin=9.49

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Spatial Deviation for Payload (250) and Speed (3)

Spatial Deviation (in .001 inches)

| Cycle | @x | @y | @z | @SQRT(@x^2+@y^2+@z^2) |
|-----------------|------|------|------|-----------------------|
| 1 | 0 | 0 | 0 | 0 |
| 2 | -0.2 | 1.1 | 0.5 | 1.2247 |
| 3 | -0.7 | 2.8 | 7.7 | 8.2231 |
| 4 | -1.2 | 4.7 | 14 | 14.816 |
| 5 | -1.5 | 4.4 | 16.7 | 17.334 |
| 6 | -1.7 | 4.9 | 18.5 | 19.213 |
| 7 | -1.7 | 5.4 | 21.6 | 22.329 |
| 8 | -1.5 | 5.3 | 21.5 | 22.194 |
| 9 | -1.4 | 5.8 | 22.4 | 23.181 |
| 10 | -1.1 | 6 | 20.6 | 21.484 |
| 11 | -0.9 | 6.4 | 20.3 | 21.303 |
| 12 | -0.9 | 7 | 17.4 | 18.776 |
| 13 | -0.7 | 8 | 14.7 | 16.750 |
| 14 | -0.7 | 8.5 | 13.1 | 15.631 |
| 15 | -0.6 | 8.9 | 11.5 | 14.554 |
| 16 | -0.6 | 10.7 | 12.1 | 16.163 |
| 17 | -0.5 | 9.9 | 9.7 | 13.869 |
| 18 | -0.9 | 9.9 | 9.3 | 13.612 |
| 19 | -0.8 | 10.3 | 8.8 | 13.570 |
| 20 | -0.4 | 10.7 | 9.9 | 14.582 |
| 21 | -0.3 | 10.9 | 8.2 | 13.643 |
| 22 | -0.2 | 11.7 | 7.4 | 13.845 |
| 23 | -0.6 | 12.9 | 7.6 | 14.984 |
| 24 | -0.8 | 12.7 | 4.7 | 13.565 |
| 25 | 11.6 | 12.9 | 6.6 | 18.561 |
| 26 ⁻ | 11.6 | 13 | 5.3 | 18.211 |
| 27 | 11.6 | 13.6 | 3.5 | 18.214 |
| 28 | 11 | 13.8 | 2.5 | 17.823 |
| 29 | 10.7 | 13.7 | 1.6 | 17.456 |
| 30 | 11 | -22 | 1 | 24.617 |

Note. @D=(@D1+@D2+...+@D30)/30=17.51 R=@Dmax-@Dmin=24.62

Cycle

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Spatial Deviation for Payload (65) and Speed (5)

Spatial Deviation (in .001 inches) _____ (ax) (ay) (az) $(ax^{2}+(ay^{2}+(az^{2})))$

| 1 | 0 | 0 | 0 | 0 |
|-----------------|-----|------|------|--------|
| 1 2 3 | 0.5 | 1.8 | 3.1 | 3.6193 |
| 3 | 1 | 2.2 | 6.1 | 6.5612 |
| 4 | 1.8 | 4.1 | 7.4 | 8.6492 |
| 5 | 2.4 | 4.2 | 8.2 | 9.5205 |
| 6 | 2.8 | 6.6 | 8 | 10.742 |
| 7 | 3.5 | 7.4 | 8.6 | 11.873 |
| 8 | 4 | 11 | 9.5 | 15.074 |
| 9 | 4.2 | 14.2 | 10 | 17.868 |
| 10 | 4.7 | 16.4 | 11.8 | 20.743 |
| 11 | 4.8 | 18.7 | 12 | 22.731 |
| 12 | 5.3 | 21.7 | 15 | 26.906 |
| 13 | 5.4 | 23.1 | 16.2 | 28.726 |
| 14 | 5.6 | 24 | 18 | 30.518 |
| 15 | 5.4 | 26.1 | 16.2 | 31.189 |
| 16 | 5.5 | 23.4 | 20.8 | 31.787 |
| 17 | 6 | 26.2 | 20.5 | 33.803 |
| 18 | 6 | 26.2 | 21.1 | 34.170 |
| 19 | 7.4 | 20.2 | 24 | 32.230 |
| 20 | 3.1 | 42.3 | 0 | 42.413 |
| 21 | 3 | 51.3 | 1 | 51.397 |
| 22 | 4.4 | 33.2 | 5.9 | 34.006 |
| 23 | 8 | 21.7 | 21.3 | 31.441 |
| 24 | 8.2 | 23.7 | 24.3 | 34.920 |
| 25 | 8.4 | 26.3 | 24.9 | 37.178 |
| 26 ⁻ | 8.2 | 27.8 | 26.2 | 39.070 |
| 27 | 7.6 | 38 | 20.1 | 43.655 |
| 28 | 7.6 | 36.2 | 22.1 | 43.088 |
| 29 | 7.7 | 38.1 | 23 | 45.165 |
| 30 | 7.8 | 35.7 | 22.5 | 42.913 |
| 31 | 7.4 | 35.3 | 23.4 | 42.993 |
| 32 | 7.4 | 36.8 | 23.5 | 44.286 |
| 33 | 8 | 38.3 | 25.9 | 46.922 |
| 34 | 8.3 | 36.2 | 26.3 | 45.508 |
| 35 | 8.2 | 35.6 | 22.2 | 42.748 |
| | | | | |

Table 18 (Continued)

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Spatial Deviation for Payload (65) and Speed (5)

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Spatial Deviation (in .001 inches)

| Cycle | @x | @y | @z | +@SQRT(@x^2+@y^2+@z^2) |
|--------|-----|------|------|------------------------|
| 36 | 8.2 | 34.1 | 23.1 | 41.995 |
| 37 | 8.1 | 38.6 | 25.1 | 46.750 |
| 38 | 8.7 | 36.4 | 23.6 | 44.244 |
| 39 | 8.4 | 37.3 | 22 | 44.111 |
| 40 | 8.4 | 35.1 | 24.6 | 43.677 |
| 41 | 8.6 | 36.5 | 27 | 46.208 |
| 42 | 8.6 | 34.2 | 25 | 43.227 |
| 43 | 8.6 | 35.2 | 25.5 | 44.308 |
| 44 | 8.5 | 33.6 | 27 | 43.934 |
| 45 | 8.6 | 36.6 | 26.8 | 46.170 |
| 46 | 8.8 | 36.2 | 26.9 | 45.950 |
| 47 | 8.9 | 35.4 | 26.4 | 45.048 |
| 48 | 9 | 34.2 | 25 | 43.308 |
| 49 | 8.9 | 34.4 | 25 | 43.446 |
| 50 | 9 | 35.2 | 25 | 44.102 |

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Spatial Deviation for Payload (65) and Speed (7)

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Spatial Deviation (in .001 inches)

| Cycle | @x | @y | @z | +@SQRT(@x^2+@y^2+@z^2) |
|-----------------|-------|------|-------------|------------------------|
| 1 | 0 | 0 | 0 | 0 |
| 2 | 0.4 | 1.4 | 5.7 | 5.8830 |
| 3 | 0.6 | 3 | 9 | 9.5057 |
| 4 | 1.8 | 4.9 | 8 | 9.5524 |
| 5 | 2.2 | 3.1 | 11.8 | 12.397 |
| 6 | 2.4 | 3.6 | 14.5 | 15.131 |
| 7 | 2.5 | 4 | 13.3 | 14.111 |
| 8 | 2.9 | 3.7 | 13.9 | 14.673 |
| 9 | 3 | 4.4 | 14.7 | 15.634 |
| 10 | 3.2 | 4.9 | 13.6 | 14.805 |
| 11 | 3.4 | 9 | 10.8 | 14.463 |
| 12 | 3.6 | 10.7 | 9.7 | 14.884 |
| 13 | 3.7 | 9.9 | 10.7 | 15.039 |
| 14 | 4 | 10.7 | 10 | 15.181 |
| 15 | 3.9 | 11.4 | 6.8 | 13.835 |
| 16 | 4.1 | 11 | 7.5 | 13.930 |
| 17 | 4.4 | 12.3 | 6.8 | 14.727 |
| 18 | 4.4 | 13.3 | 6.3 | 15.360 |
| 19 | _ 4.4 | 13.9 | 6.6 | 16.004 |
| 20 | 4.4 | 12.7 | 6.8 | 15.062 |
| 21 | 4.6 | 14.7 | 8.2 | 17.449 |
| 22 | 4.5 | 13.4 | 9.8 | 17.200 |
| 23 | 4.8 | 13.4 | 9.3 | 17.002 |
| 24 | 4.9 | 15.7 | 10.6 | 19.566 |
| 25 | 4.9 | 15.9 | 10.5 | 19.674 |
| 26 ⁻ | 5 | 14.8 | 10 | 18.548 |
| 27 | 5.1 | 15.1 | 9.8 | 18.709 |
| 28 | 5.1 | 17.8 | 9.7 | 20.903 |
| 29 | 5.2 | 17.1 | 9 .7 | 20.335 |
| 30 | 5.3 | 18.5 | 9.6 | 21.505 |
| 31 | 5.4 | 17.7 | 9.6 | 20.847 |
| 32 | 5.4 | 17.9 | 9.8 | 21.109 |
| 33 | 5.5 | 18.4 | 9.3 | 21.337 |
| 34 | 5.6 | 19.4 | 9.7 | 22.401 |
| 35 | 5.7 | 18.1 | 9.7 | 21.311 |

Table 19 (Continued)

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Spatial Deviation for Payload (65) and Speed (7)

Spatial Deviation (in .001 inches)

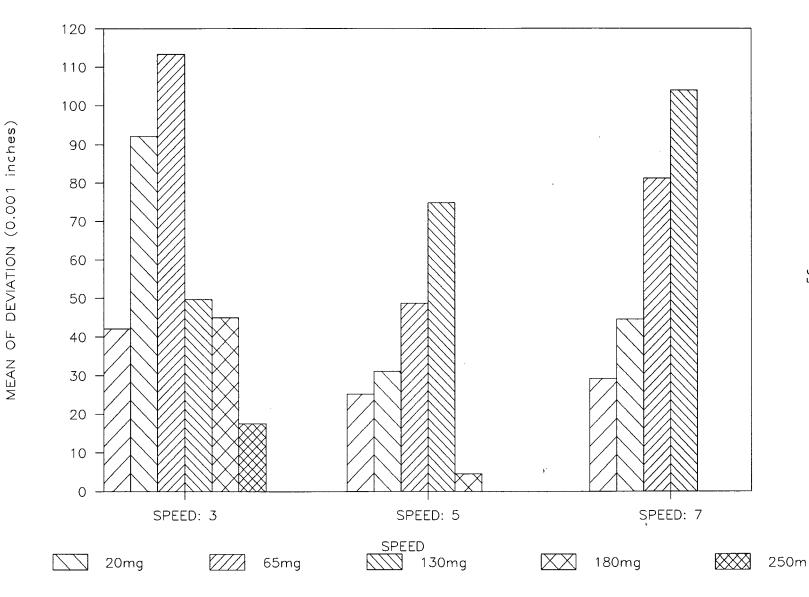
| Cycle | @x | @y | @z | +@SQRT(@x^2+@y^2+@z^2) |
|-------|-----|--------------|------|------------------------|
| 36 | 5.7 | 17.8 | | 21.389 |
| 37 | 5.8 | 17.7 | 9.1 | 20.730 |
| 38 | 5.9 | 18.7 | 10.7 | 22.338 |
| 39 | 6 | 18.9 | 10.6 | 22.484 |
| 40 | 6 | 17.9 | 10 | 21.363 |
| 41 | 6.1 | 16.9 | 9.9 | 20.514 |
| 42 | 6.1 | 18.2 | 10.8 | 22.024 |
| 43 | 6.2 | 17.8 | 10.9 | 21.773 |
| 44 | 6.2 | 17.4 | 11 | 21.498 |
| 45 | 6.3 | 17. 9 | 11 | 21.933 |
| 46 | 6.4 | 18.1 | 10.8 | 22.027 |
| 47 | 6.4 | 17.9 | 12.3 | 22.641 |
| 48 | 6.4 | 18 | 11.9 | 22.507 |
| 49 | 6.7 | 17 | 11.8 | 21.751 |
| 50 | 6.4 | 17.9 | 11.9 | 22.427 |

Analysis of Mean Deviation "@D" and Range of Deviation "R"

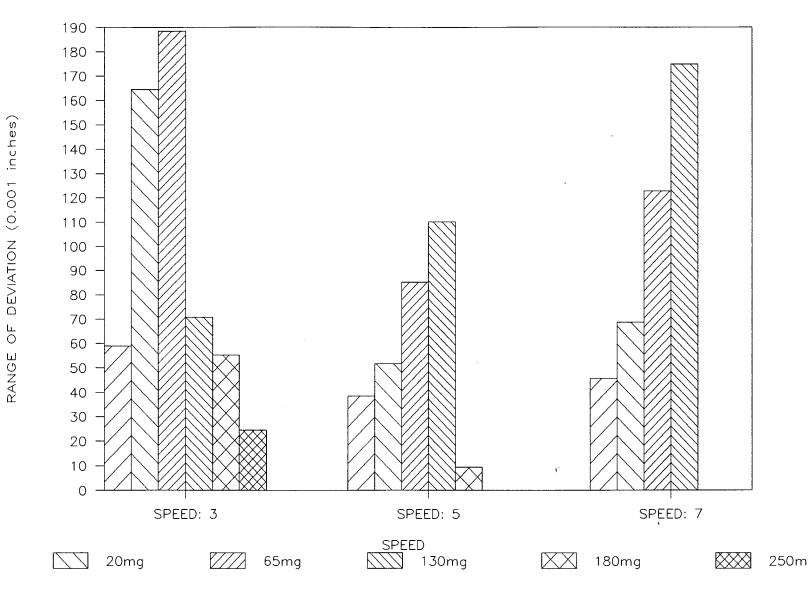
The "@D" and "R" were arranged into two groups. One group of data was organized to show the affect of different speeds on repeatability (see Figure 3 and Figure 4). For the same payload, both high speed (7) and lower speed (3) caused higher spatial position deviation than medium speed (5). This means that the medium speed could have better repeatability than higher speed or lower speed.

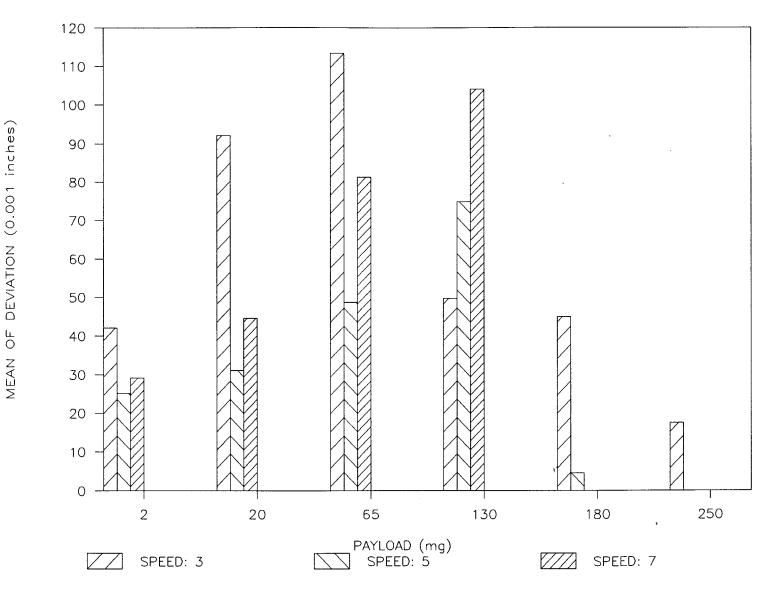
Another group was organized to show the effect of different payloads on repeatability (see Figure 5 and Figure 6). It was found that under the same speed, heavier payload caused greater spatial position deviation, i.e., the heavier the payload, the lower the repeatability. Two heavy payloads: 180gm and 250gm gave an opposite result. Because it was very difficult to read the readings from dial-indicators at the beginning of the test, the researcher had to begin recording after few cycles. However, the researcher observed that the first few cycles of high payload had greater deviation, then quickly came to a modest change rate. Both "QD" and "R" can give the same conclusion.

FIGURE 3. Mean Of Deviation (@D)



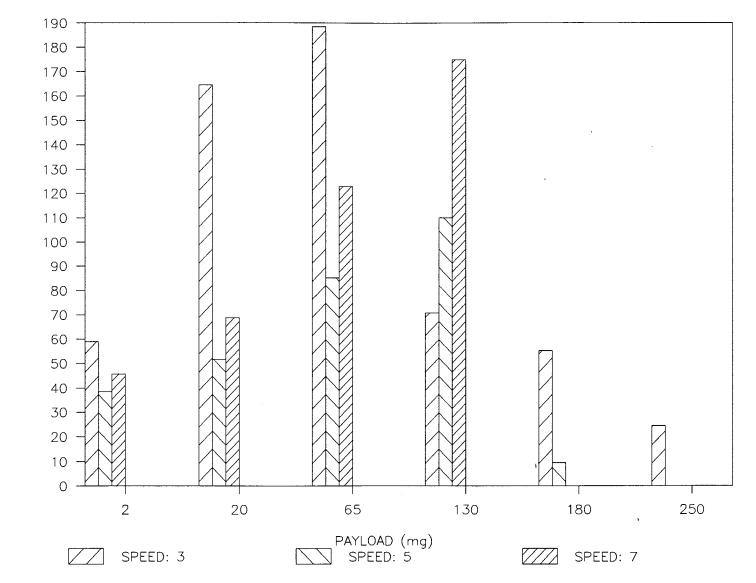






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FIGURE 6. Range Of Deviation (R)



RANGE OF DEVIATION (0.001 inches)

Analysis of Change Rate of Deviation "b"

and Coefficient of Correlation "r"

The analysis of "b" and "r" can give readers an idea about the spatial position deviation change during the cycle period and how these deviations were distributed. The "b" showed the direction of change, and the "r" showed the correlation of data. Therefore, "b" and "r" represented how the repeatability changed. Table 18 and Table 19 summarized "b" and "r" as shown in Appendix C. It is known that r=1 represents high positive correlation, and r=0 represents no correlation. Payloads of 2-130 gm exhibited higher correlation while the higher payloads of 180gm and 250gm yielded lower correlation results. This means that the repeatability of higher payloads fluctuated. Slope "b" values in table 18 demonstrated that the lower speed (3) had the highest change rate, and medium speed (5) had the lowest change rate. This also indicated that medium speed had good repeatability. Figure 7 to Figure 15 show the whole view of repeatability changes.

TABLE 20:

Summary of the Change Rate of Deviation Slope

| SPREDS | PAYLOAD (GRAMS) | | | | | | |
|--------|-----------------|------|------|------|------|-----|--|
| | 2 | 20 | 65 | 130 | 180 | 250 | |
| 3 | 1.98 | 5.82 | 6.41 | 1.85 | 0.45 | 0.2 | |
| 5 | 1.20 | 1.65 | 2.88 | 3.52 | 0.04 | | |
| 7 | 1.50 | 2.30 | 3.86 | 6.36 | | | |

Note: Unit = 0.001 inches.

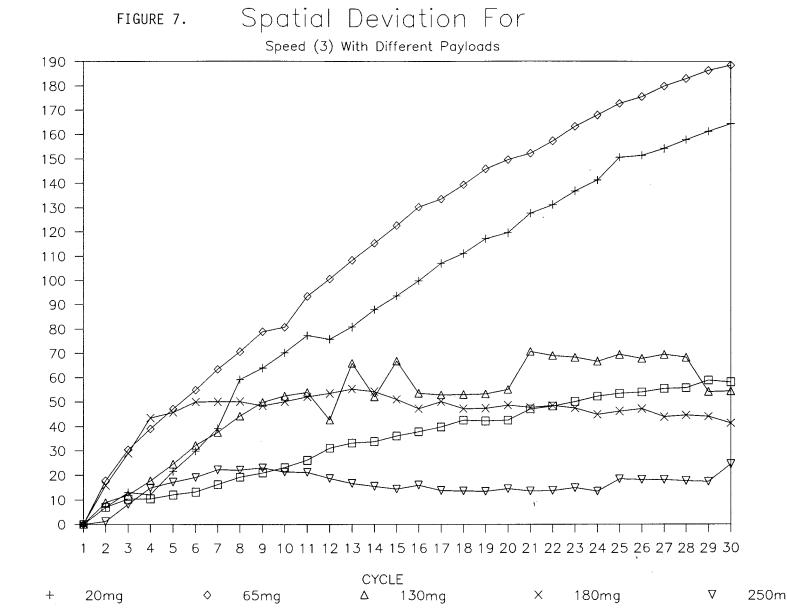
The rows show the payload's effect on the repeatability with a certain speed. The columns show the speed's effect on repeatability with a certain payload.

TABLE 21:

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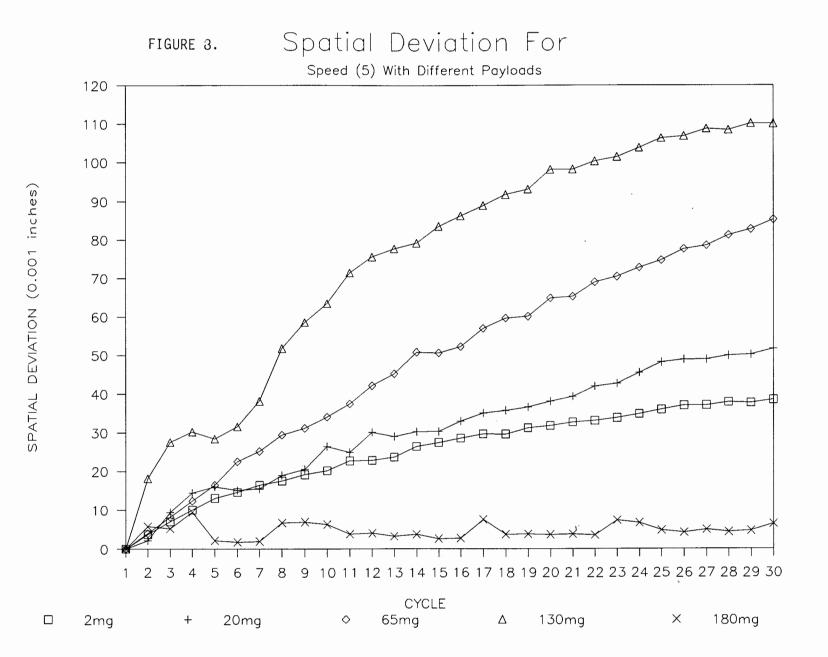
Summary of the Coefficient of Correlation "r"

| SPEEDS | PAYLOAD (GRAMS) | | | | | | | |
|--------|-----------------|------|------|------|------|-----|--|--|
| | 2 | 20 | 65 | 130 | 180 | 250 | | |
| 3 | 0.99 | 0.99 | 0.98 | 0.82 | 0.35 | 0.3 | | |
| 5 | 0.97 | 0.98 | 0.99 | 0.95 | 0.16 | | | |
| 7 | 0.96 | 0.96 | 0.96 | 0.98 | | | | |



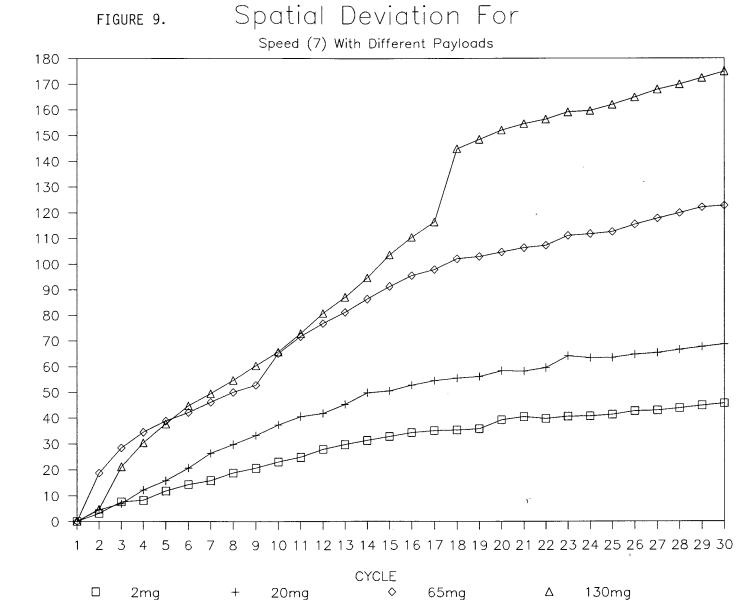
.

SPATIAL DEVIATION (0.001 inches)



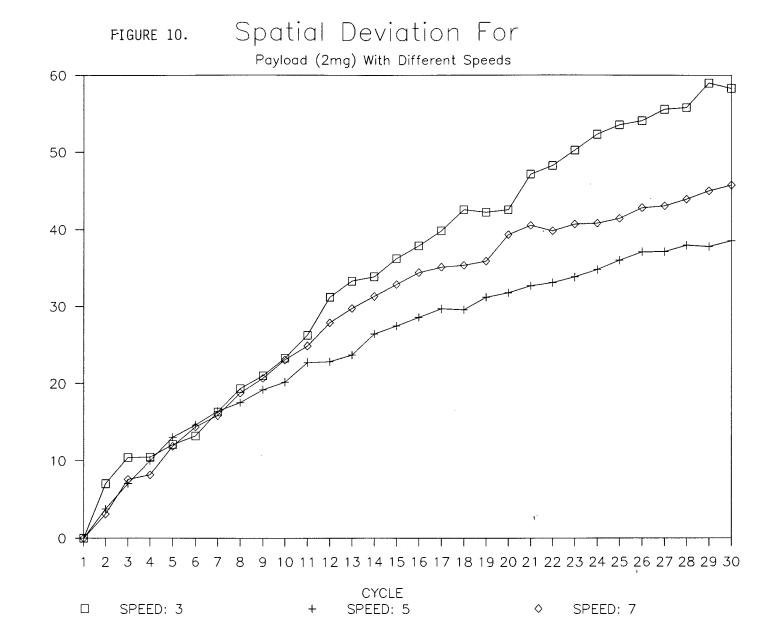
63

.



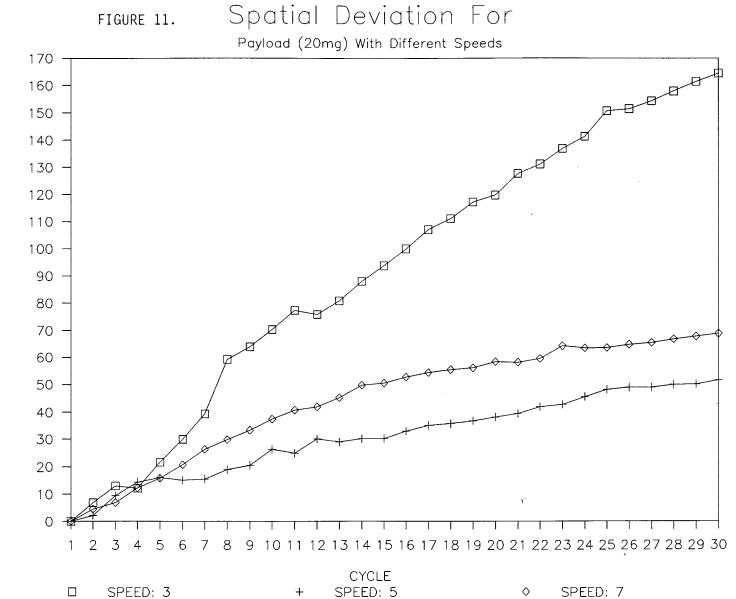
64

.



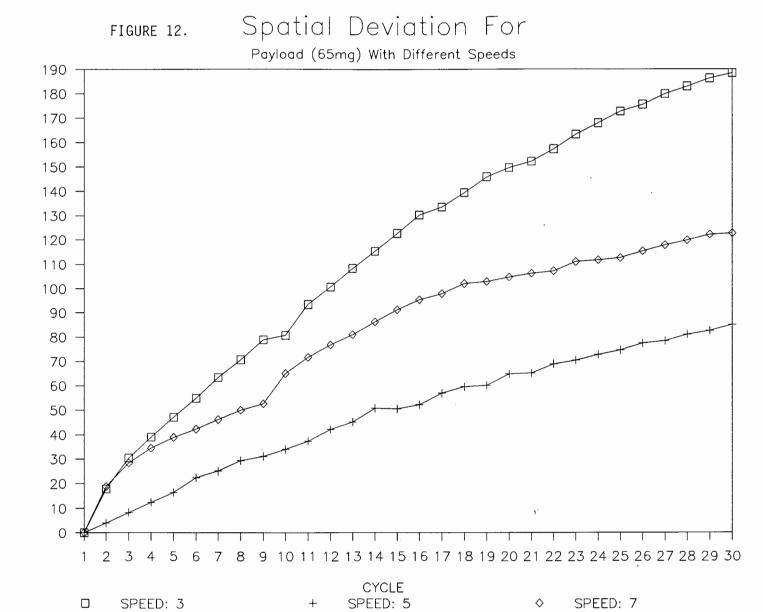
.

SPATIAL DEVIATION (0.001 inches)



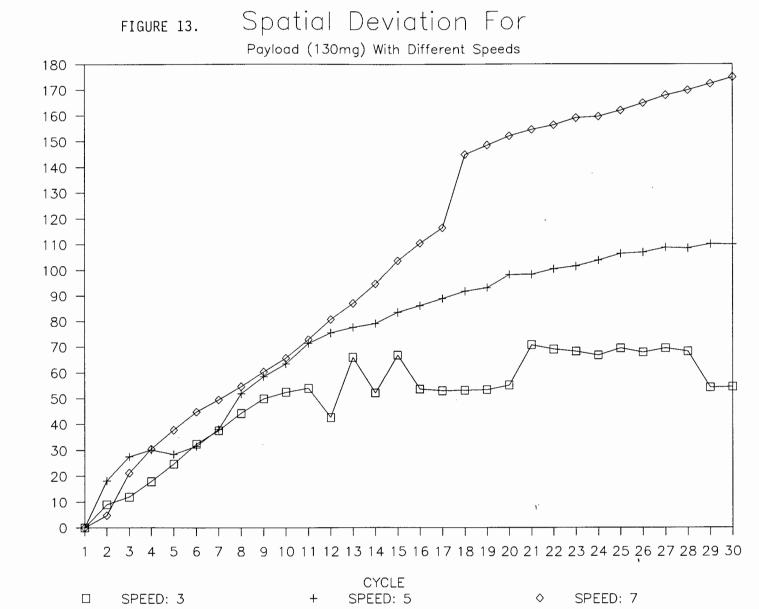
66

.



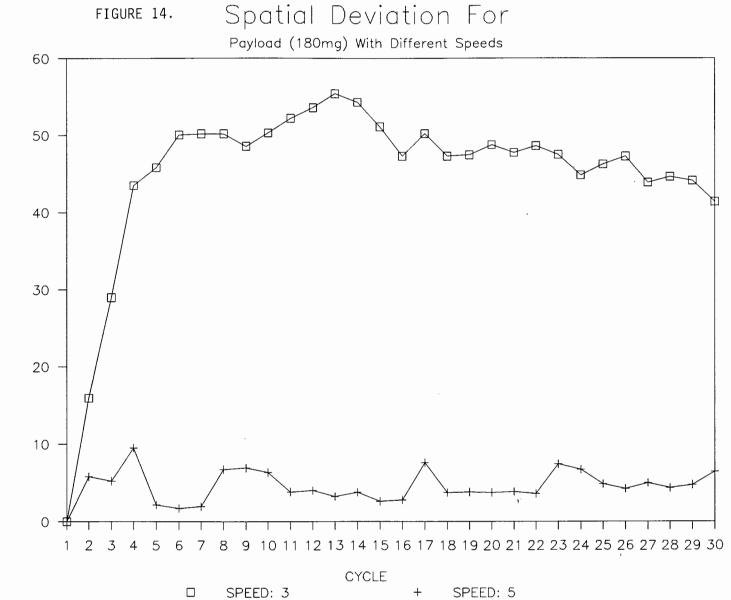
67

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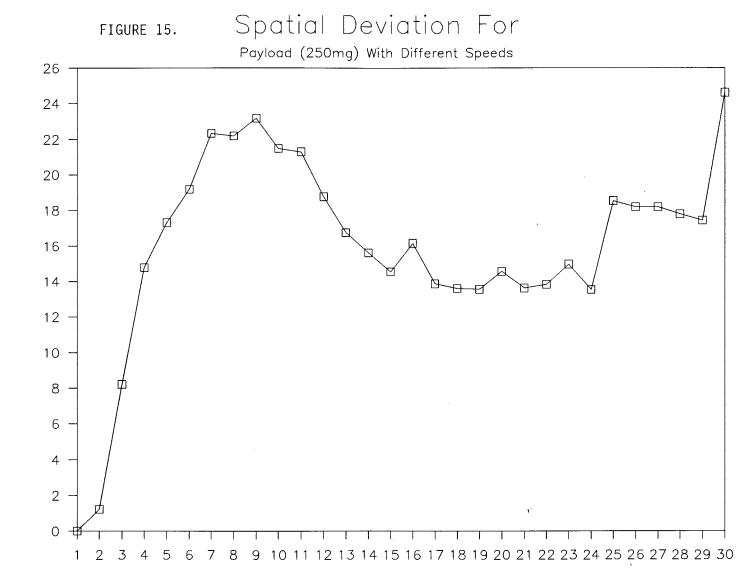
63

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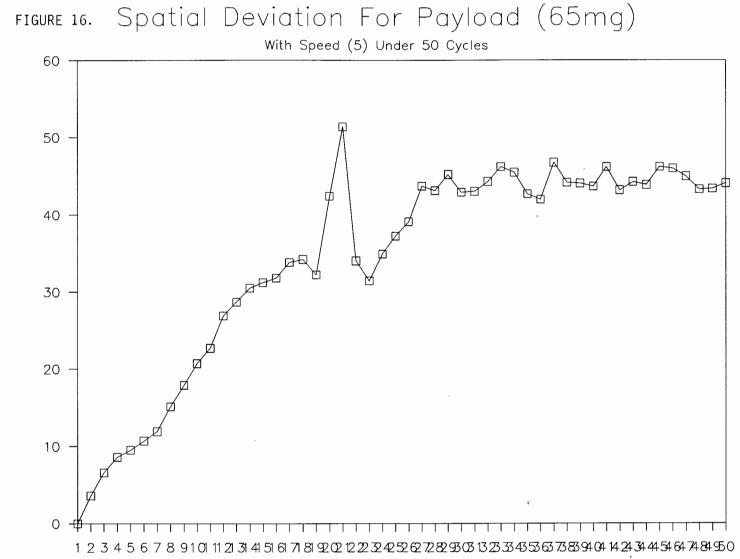
,

CYCLE

.

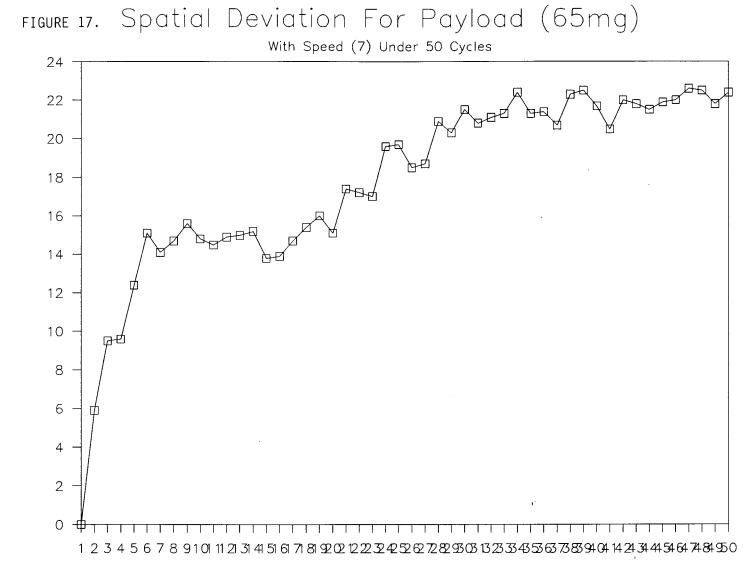
From Figure 7 to Figure 15, it can be seen that during the thirty cycles, the spatial deviation is always going up. Figure 16 and Figure 17 show the spatial deviation change of payload 65 with speed 5 and speed 7 during 50 cycles.

In Figure 16, the line becomes smoothly flat after 40 cycles. In Figure 17, during the last few cycles, the spatial deviation value have almost no change. These results suggest that the spatial deviation will tend to have low variability as the number of cycles increases. This limitation depends on the configuration or the structure of robots. The driving and the transmission system can especially affect this change of spatial deviation or repeatability. In this study, the researcher used the Microbot. It is equipped with a cable-type transmission system. Under a certain load and speed, this cable is exerted by load, weight or inertial force. Even though its length can be extended, it should have a certain limitation up to which no more significant change occurs.



SPATIAL DEVIATION (0.001 inches)

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CYCLE

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CHAPTER VI

SUMMARY, CONCLUSION AND RECOMMENDATION

Summary

Industrial robots have typically been used as general purpose positioning devices. In such a situation, the robot is programmed to move through a sequence of positions so that a tool or part held by the robot completes a desired task on a workpiece. The most important requirement for successful accomplishment of its task is the repeatability with which it can return to the taught positions and with which successive workpieces can be presented to it (Taylor, 1985).

The purpose of this research was to identify key factors that can affect the accuracy and repeatability of the Microbot TeachMover robot. There are various factors which may affect the repeatability of a given robot. The problem of this research was to determine how the factors of payload and speed affect the repeatability of a Microbot TeachMover robot. In this study, the repeatability was analyzed in terms of "QD",

"R", "r" and "b" ("@D" = spatial deviation; "R" = range of spatial deviation; "r" = coefficient of correlation; and "b" = changing rate of the spatial deviation or slope.

This research was conducted in the CAM Lab of the Industrial Technology Center, University of Northern Iowa. The Microbot TeachMover Robot that was used for this research had been used for about five years, which is a limitation of this study.

The robot program was developed using the standard teach pendent, and stored on a 5 1/4" floppy disc. The same program was used repeatedly with different payloads and different speeds. There were fifteen pairs of payload and speed run under thirty cycles, and two pairs of payload and speed run under fifty cycles. Three dial-indicators were set together to measure the position deviation on X, Y, and Z axis separately. Then the spatial deviation @D was calculated with the formula: @D = SQRT {(@X)^2+(@Y)^2+(@Z)^2}. "R" was calculated with the formula: R = @D(maximum)-@D(minimum).

In order to separately analyze the effect of payload and speed on repeatability, the " $\overline{\text{(D)}}$ " and "R"

were arranged into two groups. One group of data was organized to show the effect of different speeds on repeatability. For the same payload, both high speed and lower speed caused higher spatial deviation than did the medium speed. Another group was organized to show the effect of different payloads on repeatability. It was found that under the same speed, heavier payload caused greater spatial position deviation. The payload 65 with speed 5 and 7 were tested under fifty cycles. These results showed that after certain cycles, the deviation or the repeatability become stable, while they always increase before thirty cycles.

All of the results from this research can add important information about the repeatability of robots. "It will require joint efforts from users, manipulators, and researchers to achieve the most productive use of [an] accurate robot system" (Day, 1988, p. 9).

Discussion and Conclusion

From previous analysis, it was concluded that medium speed and light payload resulted in better repeatability. When the robot held heavier payload and ran at low speed or at high speed, the repeatability

became worse. The repeatability (or the spatial deviation in this study) changes cycle by cycle. But up to a certain degree (or certain cycles), there was almost no change in repeatability.

According to the physical configuration, the Microbot used for this study falls into the articulating configuration. It has five degrees of freedom, and five axes provide its basic motions. DC stepper-motors of the open-loop type are used to drive each of the axes of motion.

The mechanical transmissions used in the Microbot can be categorized into cable type transmissions. All motors are connected to a common drive shaft, and then the cables are connected through gears to drive different elements of the robot. Backlash and unstable characteristics are main disadvantages of the cables which contribute much to inaccuracy and poor repeatability.

Dynamic parameters such as force, gravity, and inertia are important in accurate robot controls. Structurally, robots are designed to be more flexible. Being flexible, robots will deflect under the load and under their own weight. There are several components

in robots that contribute to flexibility, such as link structures, bearings, and drive train components. They all contribute to robot inaccuracy when payloads change at the robot end effector. The heavier the payload, the more the inaccuracy. The researcher also believes that when speed becomes slower for the same payload, the time the payload is exerted on the robot will be longer, and will create more inaccuracy or irrepeatability. But when speed is high, it will come to another problem. The higher the speed, the larger the inertial force accumulates and the worse its repeatability.

Inertial parameters of robots play a role in trajectory accuracy and velocity accuracy of robots. With inertia and flexibility in a dynamic system, there are resonance or natural liberation. The robot shakes at or near its natural frequencies. When a robot holds a heavy payload, the amplitude of vibration becomes low. This is why heavy payload in this study showed lower "b".

The friction parameters of robots also contribute to the robot's inaccuracy and poor repeatability. Hysteriosis shows up when the drive cycled back and

forth, thus contributing errors in omnidirectional repeatability, and accuracy. All friction parameters dissipate energy and contribute to robot inaccuracy.

In order to build a high-quality robot to meet the more rigorous requirements in the modern industrial environment, people should do more patient work on the improvement of robot, and reveal more and more secrets of robots.

Rcommendations

The following recommendations were suggested as a result of this research project:

- The variable program complexity should be considered when conducting future studies.
- Researching on the repeatability of industrial robots should be conducted in the manufacturing system.
- Researchers could use more precise measurement techniques, such as the laser tracking system, to study path repeatability rather than point repeatability.
- 4. Different types of robots should be studied to compare their repeatability.
- 5. Research should focus on a specific part of the

robot, such as base rotation, shoulder flex, elbow flex, wrist pitch or wrist roll, to study how this part affects the repeatability of a robot.

REFERENCES

- Asfahl, C. R. (1985). <u>Robots and Manufacturing</u> <u>Automation</u>. New York: John Wiley & Sons.
- Andeen, G.B. (1988). <u>Robot Design Handbook</u>. New York: McGraw-Hill Book Company.
- Atkeson, C.G., An, C.H. & Hollerbach, J.M. (1986). Estimation of inertial parameters of manipulator loads and links. In O.D. Faugeras & Georges Giralt (ed.), <u>Robotics Research</u> (pp. 221-228) London: The MIT Press.
- Day, C. P. (1988). Robot accuracy issues and methods of improvement. <u>Robotics Today</u>, <u>1</u>, 1-9.
- Heath, L. (1986). <u>Microbot</u>. Sunnyvale, CA: Microbot, Inc.
- Heath, L. (1985). <u>Fundamentals of Robotics: Theory and</u> <u>Applications</u>. Virginia: Reston Publishing Company.
- Hollerbach, J. M. (1982). Dynamics. In Michael Brady, John M. Hollerbach, Timothy L. Johnson, Tomas Lozano-Perez & Matthew T. Mason (ed.), <u>Robot Motion</u> (pp. 51-71). Cambridge: The MIT Press.
- Holzbock, W. G. (1986). <u>Robotic Technology</u>. New york: Van Nostrand Reinhold.
- Hunt, V. D. (1990). <u>Understanding Robotics</u>. New York: Academic Press, INC.
- Kafrissen, E & Stephans, M. (1984). Industrial Robots and Robotics. Virginia: Reston Publishing company, Inc.
- Koren, Y. (1985). <u>Robotics for Engineers</u>. New York: McGraw-Hill Book Company.
- Mason, M.T. (1985). <u>Robot Hands and the Mechanics of</u> <u>Manipulation</u>. London, England: The MIT Press.

- McDonald, A. C. (1986). <u>Robot Technology: Theory</u>, <u>Design and Applications</u>. New Jersey: Prentice-Hall.
- N-Nagy & Siegler, A. (1987). <u>Engineering Foundations of</u> <u>Robotics</u>. NJ: Prentice-Hall International.
- Poole, H. H. (1989). <u>Fundamentals of Robotics</u> <u>Engineering</u>. New York: Van Nostrand Reinhold.
- Rivin, E.I. (1988). <u>Mechanical Design of Robots</u>. New York: McGraw-Hill Book Company.
- Stonecipher, K. (1989). Understanding the complex components of robot systems. In Ken Stonecipher (ed.), <u>Industrial robotics</u> (pp.1-33). Indiana: Howard W. Sams & Company.
- Taylor, R.H.; Hollis, R.L.; Lavin, M.A. (1985). Precise manipulation with endpoint sensing. <u>IBM</u> <u>Journal of Research and Development, 29</u>, 363-376.
- Tracking system measures continuous path robot motions (1985). <u>Production Engineering</u>, <u>32</u>, 15.
- Vukobratovic, M & Potkonjak, V. (1985). Scientific Fundamentals of Robotics 6: Applied Dynamics and CAD of Manipulation Robots. New York: Springer-Verlag.

APPENDIX A

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The Program of Microbot for this Research

PROGRAM FOR SPEED 3

STEP COMMAND OPERANDS

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| 0 | MOVE | 183,0,0,0,0,0,0 |
|----|-------|---|
| 1 | PAUSE | 12 |
| 2 | MOVE | 183,-51,-361,73,0,0,73 |
| 3 | MOVE | 183,-51,-873,264,0,0,264 |
| 4 | MOVE | 183,-51,-873,578,385,385,578 |
| 5 | MOVE | 183,1763,-873,578,385,385,578 |
| 6 | MOVE | 183,1763,-1183,-240,168,168,-240 |
| 7 | MOVE | 183,-1752,-1183,-240,168,168,-240 |
| 8 | MOVE | 183,-1752,-2009,-1297,-412,-412,-1297 |
| 9 | MOVE | 183, -14, -2009, -1297, -412, -412, -1297 |
| 10 | MOVE | 183,-14,-915,542,405,405,542 |
| 11 | MOVE | 183,-14,-915,542,1151,-341,542 |
| 12 | MOVE | 183,-14,-915,542,68,742,542 |
| 13 | MOVE | 183,-14,-915,542,425,385,542 |
| 14 | MOVE | 183,1743,-915,542,425,385,542 |
| 15 | MOVE | 183,1743,-1605,0,425,385,0 |
| 16 | MOVE | 183,-1707,-1605,0,425,385,0 |
| 17 | MOVE | 183,-1707,-817,674,408,368,674 |
| 18 | MOVE | 183,-18,-817,674,408,368,674 |
| 19 | MOVE | 183,-18,-817,674,731,45,674 |
| 20 | MOVE | 183,-18,-817,674,-38,814,674 |
| 21 | MOVE | 183,-18,-817,674,433,343,674 |
| 22 | MQVE | 183,-18,-699,276,36,-54,276 |
| 23 | MOVE | 183,-52,-366,83,-19,1,83 |
| | | |

PROGRAM FOR SPEED 5

STEP COMMAND OPERANDS

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| 0 | MOVE | 183,0,0,0,0,0,0 |
|----|-------|---------------------------------------|
| 1 | PAUSE | 12 |
| 2 | MOVE | 221,-51,-361,73,0,0,73 |
| 3 | MOVE | 221,-51,-873,264,0,0,264 |
| 4 | MOVE | 221,-51,-873,578,385,385,578 |
| 5 | MOVE | 221,1763,-873,578,385,385,578 |
| 6 | MOVE | 221,1763,-1183,-240,168,168,-240 |
| 7 | MOVE | 221,-1752,-1183,-240,168,168,-240 |
| 8 | MOVE | 221,-1752,-2009,-1297,-412,-412,-1297 |
| 9 | MOVE | 221,-14,-2009,-1297,-412,-412,-1297 |
| 10 | MOVE | 221,-14,-915,542,405,405,542 |
| 11 | MOVE | 221,-14,-915,542,1151,-341,542 |
| 12 | MOVE | 221,-14,-915,542,68,742,542 |
| 13 | MOVE | 221,-14,-915,542,425,385,542 |
| 14 | MOVE | 221,1743,-915,542,425,385,542 |
| 15 | MOVE | 221,1743,-1605,0,425,385,0 |
| 16 | MOVE | 221,-1707,-1605,0,425,385,0 |
| 17 | MOVE | 221,-1707,-817,674,408,368,674 |
| 18 | MOVE | 221,-18,-817,674,408,368,674 |
| 19 | MOVE | 221,-18,-817,674,731,45,674 |
| 20 | MOVE | 221,-18,-817,674,-38,814,674 |
| 21 | MOVE | 221,-18,-817,674,433,343,674 |
| 22 | MOVE | 221,-18,-699,276,36,-54,276 |
| 23 | MOVE | 221,-52,-366,83,-19,1,83 |

PROGRAM FOR SPEED 7

STEP COMMAND OPERANDS

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| 0 | MOVE | 183,0,0,0,0,0,0 |
|----|-------|---|
| 1 | PAUSE | 12 |
| 2 | MOVE | 236,-51,-361,73,0,0,73 |
| 3 | MOVE | 236,-51,-873,264,0,0,264 |
| 4 | MOVE | 236, -51, -873, 578, 385, 385, 578 |
| 5 | MOVE | 236,1763,-873,578,385,385,578 |
| 6 | MOVE | 236,1763,-1183,-240,168,168,-240 |
| 7 | MOVE | 236, -1752, -1183, -240, 168, 168, -240 |
| 8 | MOVE | 236, -1752, -2009, -1297, -412, -412, -1297 |
| 9 | MOVE | 236, -14, -2009, -1297, -412, -412, -1297 |
| 10 | MOVE | 236,-14,-915,542,405,405,542 |
| 11 | MOVE | 236,-14,-915,542,1151,-341,542 |
| 12 | MOVE | 236,-14,-915,542,68,742,542 |
| 13 | MOVE | 236,-14,-915,542,425,385,542 |
| 14 | MOVE | 236,1743,-915,542,425,385,542 |
| 15 | MOVE | 236,1743,-1605,0,425,385,0 |
| 16 | MOVE | 236,-1707,-1605,0,425,385,0 |
| 17 | MOVE | 236,-1707,-817,674,408,368,674 |
| 18 | MOVE | 236,-18,-817,674,408,368,674 |
| 19 | MOVE | 236,-18,-817,674,731,45,674 |
| 20 | MOVE | 236,-18,-817,674,-38,814,674 |
| 21 | MOVE | 236,-18,-817,674,433,343,674 |
| 22 | MQVE | 236,-18,-699,276,36,-54,276 |
| 23 | MOVE | 236,-52,-366,83,-19,1,83 |

APPENDIX B

Microbot TeachMover Characteristics

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Table ---- Microbot TeachMover Characteristics

| GENERAL | |
|--|---|
| Configuration | 5 revolution axes and integral hand |
| Drive | Electric stepper motors - Open loop control |
| Controller | 6502A microprocessor with 4K bytes of EPROM and 1K bytes of RAM located in the base of the unit |
| Interface | Dual RS-232C asynchronous serial communications interfaces (baud rate is switch-selectable between 110, 150, 300, 600, 1200, 2400, 4800, and 9600 baud) |
| Teach Control | 14-key 13-function keyboard; 5 output and 7 input bits under computer control |
| Power requirement | 12 to 14 volts, 4.5 amps DC |
| PERFORMANCE | |
| Resolution Load Capacity Gripping Force Reach Velocity | 0.011 in (0.25mm) maximum on each axis 16 oz (455 gm) at full extension 3 lbs (13 newtons) maximum 17.5 in (444 mm) 0-7 in/sec (0-178 mm/sec) with controlled acceleration |
| DETAILED PERFORMANCE | |
| Joint Max Range of Motion | Speed (full Load) Speed (No load) |
| Base $\pm 90^{\circ}$ Shoulder $+144^{\circ}$, -35° Elbow $+0^{\circ}$, -149° Wrist Roll $\pm 270^{\circ}$ Wrist Pitch $\pm 90^{\circ}$ Hand0-3 in | 0.37 rad/sec 0.42 rad/sec 0.15 rad/sec 0.36 rad/sec 0.23 rad/sec 0.82 rad/sec 1.31 rad/sec 2.02 rad/sec 1.31 rad/sec 2.02 rad/sec 20 mm/sec |
| PHYSICAL CHARACTERISTICS | |
| | |

Arm Weight Teach Control Cable Length 8 lbs (4kg) 3.75 ft.(1150 mm)

Source: Heath, L. (1986). Microbot.

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APPENDIX C

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The Result of "b" and "r" Calculated with "POM" Software Package

File: AYLOAD:2 & SPEED:3

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PAYLOAD:2 & SPEED:3

Method:Linear Regression/least squares

| | éD | Period | x^2 | х * у | Forecast | Error^2 |
|---------|----------|--------|---------|---------|----------|---------|
| cycle 1 | 0.00 | 1 | 1.00 | 0.00 | 5.74 | 32.97 |
| cycle 2 | 7.04 | 2 | 4.00 | 14.08 | 7.72191 | .465003 |
| cycle 3 | 10.40 | 3 | 9.00 | 31.20 | 9.70221 | .486904 |
| cycle 4 | 10.44 | 4 | 16.00 | 41.76 | 11.6825 | 1.54385 |
| cycle 5 | 12.11 | 5 | 25.00 | 60.55 | 13.6628 | 2.41125 |
| cycle 6 | 13.20 | 6 | 36.00 | 79.20 | 15.6431 | 5.96885 |
| cycle 7 | 16.33 | 7 | 49.00 | 114.31 | 17.6234 | 1.67295 |
| cycle 8 | 19.35 | 8 | 64.00 | 154.80 | 19.6037 | 0.06438 |
| cycle 9 | 21.00 | 9 | 81.00 | 189.00 | 21.58 | .341093 |
| cycle10 | 23.29 | 10 | 100.00 | 232.90 | 23.5643 | 0.07526 |
| cycle11 | 26.25 | 11 | 121.00 | 288.75 | 25.5446 | .497536 |
| cycle12 | 31.20 | 12 | 144.00 | 374.40 | 27.5249 | 13.51 |
| cycle13 | 33.32 | 13 | 169.00 | 433.16 | 29.5052 | 14.5524 |
| cycle14 | 33.88 | 14 | 196.00 | 474.32 | 31.4855 | 5.73341 |
| cycle15 | 36.23 | 15 | 225.00 | 543.45 | 33.4659 | 7.64052 |
| cycle16 | 37.88 | 16 | 256.00 | 606.08 | 35.4462 | 5,92362 |
| cycle17 | 39.85 | 17 | 289.00 | 677.45 | 37.4265 | 5.87356 |
| cycle18 | 42.58 | 18 | 324.00 | 766.44 | 39.4068 | 10.0695 |
| cycle19 | 42.22 | 19 | 361.00 | 802.18 | 41.39 | .693788 |
| cycle20 | 42.56 | 20 | 400.00 | 851.20 | 43.3674 | .651833 |
| cycle21 | 47.18 | 21 | 441.00 | 990.78 | 45.3477 | 3.35744 |
| cycle22 | 48.31 | 22 | 484.00 | 1062.82 | 47.3280 | .964388 |
| cycle23 | 50.30 | 23 | 529.00 | 1156.90 | 49.3083 | 0.98 |
| cycle24 | 52.36 | 24 | 576.00 | 1256.64 | 51.2886 | 1.14795 |
| cycle25 | 53.56 | 25 | 625.00 | 1339.00 | 53.2689 | 0.08475 |
| cycle26 | 54.09 | 26 | 676.00 | 1406.34 | 55.2492 | 1.34 |
| cycle27 | 55.60 | 27 | 729.00 | 1501.20 | 57.2295 | 2.65522 |
| cycle28 | 55.82 | 28 | 784.00 | 1562.96 | 59.21 | 11.4907 |
| cycle29 | 59.00 | 29 | 841.00 | 1711.00 | 61.19 | 4.79649 |
| cycle30 | 58.33 | 30 | 900.00 | 1749.90 | 63.17 | 23.4294 |
| TOTALS | 1033.68 | 465.00 | 9455.00 | 20472.8 | 65.1507 | 161.391 |
| AVERAGE | 34.456 🕤 | 15.50 | 315.167 | 682.426 | 0.00 | 5.37971 |
| | | | | | | (MSE) |

Next period forecast=65.1507Regression line = : Y =3.76 +1.98 * XCorrelation coefficient =0.9909684Standard error =2.400828



File: PAYLOAD:2 & SPEED:5

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| Mechod: PII | lear reyres | | - | _ | <u> </u> | - |
|-------------|-------------|--------|---------|---------|----------|---------|
| | @D | Period | x^2 | х * у | Forecast | Error^2 |
| cycle 1 | 0.00 | 1 | 1.00 | 0.00 | 7.74 | 59.8715 |
| cycle 2 | 3.77 | 2 | 4.00 | 7.54 | 8.93914 | 26.72 |
| cycle 3 | 7.07 | 3 | 9.00 | 21.21 | 10.1406 | 9.42865 |
| cycle 4 | 10.02 | 4 | 16.00 | 40.08 | 11.34 | 1.75 |
| cycle 5 | 13.06 | 5 | 25.00 | 65.30 | 12.5436 | .266718 |
| cycle 6 | 14.62 | 6 | 36.00 | 87.72 | 13.75 | .765582 |
| cycle 7 | 16.42 | 7 | 49.00 | 114.94 | 14.9465 | 2.17122 |
| cycle 8 | 17.53 | 8 | 64.00 | 140.24 | 16.1480 | 1.91 |
| cycle 9 | 19.17 | 9 | 81.00 | 172.53 | 17.3494 | 3.31445 |
| cycle10 | 20.16 | 10 | 100.00 | 201.60 | 18.5509 | 2.58917 |
| cycle11 | 22.71 | 11 | 121.00 | 249.81 | 19.7524 | 8.75 |
| cycle12 | 22.83 | 12 | 144.00 | 273.96 | 20.9538 | 3.52 |
| cycle13 | 23.68 | 13 | 169.00 | 307.84 | 22.1553 | 2.32465 |
| cycle14 | 26.43 | 14 | 196.00 | 370.02 | 23.36 | 9.44 |
| cycle15 | 27.46 | -15 | 225.00 | 411.90 | 24.5583 | 8.42007 |
| cycle16 | 28.57 | 16 | 256.00 | 457.12 | 25.7597 | 7.89759 |
| cycle17 | 29.69 | 17 | 289.00 | 504.73 | 26.9612 | 7.44633 |
| cycle18 | 29.58 | 18 | 324.00 | 532.44 | 28.1627 | 2.01 |
| cycle19 | 31.21 | 19 | 361.00 | 592.99 | 29.3641 | 3.41 |
| cycle20 | 31.80 | 20 | 400.00 | 636.00 | 30.5656 | 1.52370 |
| cycle21 | 32.69 | 21 | 441.00 | 686.49 | 31.77 | 0.85 |
| cycle22 | 33.11 | 22 | 484.00 | 728.42 | 32.9686 | 0.02001 |
| cycle23 | 33.83 | 23 | 529.00 | 778.09 | 34.17 | 0.12 |
| cycle24 | 34.83 | 24 | 576.00 | 835.92 | 35.3715 | .293222 |
| cycle25 | 36.00 | 25 | 625.00 | 900.00 | 36.5730 | .328296 |
| cycle26 | 37.11 | 26 | 676.00 | 964.86 | 37.7744 | .441486 |
| cycle27 | 37.15 | 27 | 729.00 | 1003.05 | 38.9759 | 3.33396 |
| cycle28 | 37.94 | 28 | 784.00 | 1062.32 | 40.18 | 5.01 |
| cycle29 | 37.78 | 29 | 841.00 | 1095.62 | 41.3789 | 12.9518 |
| cycle30 | 38.55 | 30 | 900.00 | 1156.50 | 42.5803 | 16.2435 |
| TOTALS | 754.77 | 465.00 | 9455.00 | 14399.2 | 43.7818 | 203.111 |
| AVERAGE | 25.159 | 15.50 | 315.167 | 479.975 | 0.00 | 6.77037 |
| | | | | | | (MSE) |
| | | | | | | |

Method:Linear Regression/least squares

Next period forecast=43.7818Regression line = : Y =6.54 + 1.20147 * XCorrelation coefficient =0.9700949Standard error = 2.69332



File: AYLOAD:2 & SPEED:7

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| Method:Lin | | ssion/least | | | | |
|------------|---------|-------------|---------|---------|----------|---------|
| | @D | Period(x) | x^2 | х * У | Forecast | Error^2 |
| cycle 1 | 0.00 | 1 | 1.00 | 0.00 | 7.34823 | 54.00 |
| cycle 2 | 3.15 | 2 | 4.00 | 6.30 | 8.85 | 32.5071 |
| cycle 3 | 7.60 | 3 | 9.00 | 22.80 | 10.3548 | 7.58878 |
| cycle 4 | 8.18 | 4 | 16.00 | 32.72 | 11.86 | 13.53 |
| cycle 5 | 11.86 | 5 | 25.00 | 59.30 | 13.3613 | 2.25396 |
| cycle 6 | 14.36 | 6 | 36.00 | 86.16 | 14.86 | 0.25 |
| cycle 7 | 15.83 | 7 | 49.00 | 110.81 | 16.3679 | .289294 |
| cycle 8 | 18.78 | 8 | 64.00 | 150.24 | 17.8711 | .826042 |
| cycle 9 | 20.66 | 9 | 81.00 | 185.94 | 19.3744 | 1.65275 |
| cycle10 | 23.05 | 10 | 100.00 | 230.50 | 20.8777 | 4.71899 |
| cycle11 | 24.89 | 11 | 121.00 | 273.79 | 22.3809 | 6.29534 |
| cycle12 | 27.88 | 12 | 144.00 | 334.56 | 23.8842 | 15.9663 |
| cycle13 | 29.77 | 13 | 169.00 | 387.01 | 25.39 | 19.21 |
| cycle14 | 31.31 | 14 | 196.00 | 438.34 | 26.8908 | 19.5297 |
| cycle15 | 32.88 | 15 | 225.00 | 493.20 | 28.39 | 20.1239 |
| cycle16 | 34.42 | 16 | 256.00 | 550.72 | 29.8973 | 20.4547 |
| cycle17 | 35.14 | 17 | 289.00 | 597.38 | 31.4006 | 13.9833 |
| cycle18 | 35.35 | 18 | 324.00 | 636.30 | 32.9039 | 5.98364 |
| cycle19 | 35.90 | 19 | 361.00 | 682.10 | 34.4071 | 2.22870 |
| cycle20 | 39.33 | 20 | 400.00 | 786.60 | 35.91 | 11.6937 |
| cycle21 | 40.56 | 21 | 441.00 | 851.76 | 37.4137 | 9.89943 |
| cycle22 | 39.83 | 22 | 484.00 | 876.26 | 38.9169 | .833691 |
| cycle23 | 40.71 | 23 | 529.00 | 936.33 | 40.4202 | 0.08398 |
| cycle24 | 40.82 | 24 | 576.00 | 979.68 | 41.9235 | 1.21767 |
| cycle25 | 41.45 | 25 | 625.00 | 1036.25 | 43.4268 | 3.90754 |
| cycle26 | 42.84 | 26 | 676.00 | 1113.84 | 44.93 | 4.36820 |
| cycle27 | 43.07 | 27 | 729.00 | 1162.89 | 46.4333 | 11.3118 |
| cycle28 | 43.95 | 28 | 784.00 | 1230.60 | 47.9366 | 15.8927 |
| cycle29 | 45.04 | 29 | 841.00 | 1306.16 | 49.4398 | 19.3586 |
| cycle30 | 45.76 | 30 | 900.00 | 1372.80 | 50.9431 | 26.8647 |
| TOTALS | 874.37 | 465.00 | 9455.00 | 16931.3 | 52.4464 | 346.82 |
| AVERAGE | 29.1457 | 15.50 | 315.167 | 564.378 | 0.00 | 11.5607 |
| | | | | | | (MSE) |
| | | | | | | |

Next period forecast=52.4464Regression line = : Y =5.84 + 1.50327 * XCorrelation coefficient =0.967512Standard or comparent 0.967512 Standard error = 3.519435 File: AYLOAD:20 & SPEED:3

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PAYLOAD:20 & SPEED:3

| ······································ | | | | | | |
|--|---------|-------------|---------|---------|----------|----------|
| Method:Lin | | ssion/least | | | T | T |
| _ | @D | Period(x) | x^2 | x * y | Forecast | Error^2 |
| cycle 1 | 0.00 | 1 | 1.00 | 0.00 | 7.83477 | 61.3836 |
| cycle 2 | 6.92 | 2 | 4.00 | 13.84 | 13.6504 | 45.2985 |
| cycle 3 | 13.01 | 3 | 9.00 | 39.03 | 19.47 | 41.68 |
| cycle 4 | 12.14 | 4 | 16.00 | 48.56 | 25.2817 | 172.705 |
| cycle 5 | 21.70 | 5 | 25.00 | 108.50 | 31.0974 | 88.3104 |
| cycle 6 | 29.95 | 6 | 36.00 | 179.70 | 36.91 | 48.48 |
| cycle 7 | 39.23 | 7 | 49.00 | 274.61 | 42.7287 | 12.2406 |
| cycle 8 | 59.28 | 8 | 64.00 | 474.24 | 48.5443 | 115.255 |
| cycle 9 | 64.00 | 9 | 81.00 | 576.00 | 54.3600 | 92.9305 |
| cycle10 | 70.32 | 10 | 100.00 | 703.20 | 60.1756 | 102.909 |
| cycle11 | 77.34 | 11 | 121.00 | 850.74 | 65.9912 | 128.794 |
| cycle12 | 75.85 | 12 | 144.00 | 910.20 | 71.8069 | 16.3466 |
| cycle13 | 80.86 | 13 | 169.00 | 1051.18 | 77.6225 | 10.4811 |
| cycle14 | 88.10 | 14 | 196.00 | 1233.40 | 83.44 | 21.7324 |
| cycle15 | 93.76 | - 15 | 225.00 | 1406.40 | 89.2538 | 20.3055 |
| cycle16 | 99.96 | 16 | 256.00 | 1599.36 | 95.07 | 23.92 |
| cycle17 | 107.10 | 17 | 289.00 | 1820.70 | 100.885 | 38.6245 |
| cycle18 | 111.11 | 18 | 324.00 | 1999.98 | 106.70 | 19.4411 |
| cycle19 | 117.16 | 19 | 361.00 | 2226.04 | 112.516 | 21.5627 |
| cycle20 | 119.77 | 20 | 400.00 | 2395.40 | 118.332 | 2.06759 |
| cycle21 | 127.68 | 21 | 441.00 | 2681.28 | 124.148 | 12.4769 |
| cycle22 | 131.15 | 22 | 484.00 | 2885.30 | 129.963 | 1.40806 |
| cycle23 | 136.86 | 23 | 529.00 | 3147.78 | 135.779 | 1.16851 |
| cycle24 | 141.37 | 24 | 576.00 | 3392.88 | 141.595 | 0.05048 |
| cycle25 | 150.68 | 25 | 625.00 | 3767.00 | 147.41 | 10.6907 |
| cycle26 | 151.44 | 26 | 676.00 | 3937.44 | 153.226 | 3.18967 |
| cycle27 | 154.32 | 27 | 729.00 | 4166.64 | 159.042 | 22.2937 |
| cycle28 | 157.95 | 28 | 784.00 | 4422.60 | 164.857 | 47.7104 |
| cycle29 | 161.36 | 29 | 841.00 | 4679.44 | 170.67 | 86.7303 |
| cycle30 | 164.48 | 30 | 900.00 | 4934.40 | 176.489 | 144.21 |
| TOTALS | 2764.85 | 465.00 | 9455.00 | 55925.8 | 182.304 | 1414.39 |
| AVERAGE | 92.1617 | 15.50 | 315.167 | 1864.19 | 0.00 | 47.1465 |
| | | | | - | | (MSE) |
| | | | | | | |

Next period forecast= 182.304 Regression line = : Y = 2.01912 + 5.81565 * X Correlation coefficient = 0.9908249Standard error = 7.107325 File:

AYLOAD:20 & SPEED:5

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PAYLOAD:20 & SPEED:5

Method:Linear Regression/least squares

| | ØD | Period(x) | x^2 | х * у | Forecast | Error^2 |
|---------|-----------|-----------|---------|---------|----------|---------|
| cycle 1 | 0.00 | 1 | 1.00 | 0.00 | 6.98734 | 48.8230 |
| cycle 2 | 2.19 | 2 | 4.00 | 4.38 | 8.64217 | 41.6305 |
| cycle 3 | 9.44 | 3 | 9.00 | 28.32 | 10.297 | .734443 |
| cycle 4 | 14.43 | 4 | 16.00 | 57.72 | 11.9518 | 6.14136 |
| cycle 5 | 16.02 | 5 | 25.00 | 80.10 | 13.6067 | 5.82 |
| cycle 6 | 15.07 | 6 | 36.00 | 90.42 | 15.2615 | 0.03666 |
| cycle 7 | 15.51 | 7 | 49.00 | 108.57 | 16.9163 | 1.98 |
| cycle 8 | 18.93 | 8 | 64.00 | 151.44 | 18.5711 | .128787 |
| cycle 9 | 20.52 | 9 | 81.00 | 184.68 | 20.2260 | 0.09 |
| cycle10 | 26.40 | 10 | 100.00 | 264.00 | 21.8808 | 20.4233 |
| cycle11 | 24.90 | 11 | 121.00 | 273.90 | 23.5356 | 1.86155 |
| cycle12 | 30.04 | 12 | 144.00 | 360.48 | 25.1904 | 23.5183 |
| cycle13 | 29.00 | 13 | 169.00 | 377.00 | 26.8453 | 4.64289 |
| cycle14 | 30.22 | 14 | 196.00 | 423.08 | 28.50 | 2.95808 |
| cycle15 | 30.30 | - 15 | 225.00 | 454.50 | 30.1549 | 0.02105 |
| cycle16 | 32.98 | 16 | 256.00 | 527.68 | 31.8097 | 1.36949 |
| cycle17 | 35.05 | 17 | 289.00 | 595.85 | 33.4646 | 2.51358 |
| cycle18 | 35.76 | 18 | 324.00 | 643.68 | 35.1194 | .410366 |
| cycle19 | 36.64 | 19 | 361.00 | 696.16 | 36.7742 | 0.02 |
| cycle20 | 38.08 | 20 | 400.00 | 761.60 | 38.43 | .121838 |
| cycle21 | 39.39 | 21 | 441.00 | 827.19 | 40.0839 | .481472 |
| cycle22 | 41.97 | 22 | 484.00 | 923.34 | 41.7387 | 0.05350 |
| cycle23 | 42.71 | 23 | 529.00 | 982.33 | 43.3935 | .467222 |
| cycle24 | 45.55 | 24 | 576.00 | 1093.20 | 45.0484 | .251639 |
| cycle25 | 48.24 | 25 | 625.00 | 1206.00 | 46.70 | 2.36 |
| cycle26 | 49.01 | 26 | 676.00 | 1274.26 | 48.36 | .425085 |
| cycle27 | 49.07 | 27 | 729.00 | 1324.89 | 50.0128 | .888948 |
| cycle28 | 50.00 | 28 | 784.00 | 1400.00 | 51.6677 | 2.78111 |
| cycle29 | 50.26 | 29 | 841.00 | 1457.54 | 53.32 | 9.37888 |
| cycle30 | 51.79 | 30 | 900.00 | 1553.70 | 54.9773 | 10.16 |
| TOTALS | 929.47 | 465.00 | 9455.00 | 18126.0 | 56.6321 | 190.49 |
| AVERAGE | 30.9823 - | 15,50 | 315.167 | 604.20 | 0.00 | 6.34968 |
| | | | | | | (MSE) |

Next period forecast= 56.6321 Regression line = : Y = 5.33252 + 1.65483 * X Correlation coefficient = 0.9848743Standard error = 2.608299 File: AYLOAD:20 & SPEED:7

e.

PAYLOAD:20 & SPEED:7

Method:Linear Regression/least squares

| | ÕD | Period(x) | x^2 | х * у | Forecast | Error^2 |
|---------|---------|-----------|---------|---------|----------|---------|
| cycle 1 | 0.00 | 1 | 1.00 | 0.00 | 11.24 | 126.294 |
| cycle 2 | 4.48 | 2 | 4.00 | 8.96 | 13.5344 | 81.9825 |
| cycle 3 | 6.91 | 3 | 9.00 | 20.73 | 15.8308 | 79.5804 |
| cycle 4 | 12.25 | 4 | 16.00 | 49.00 | 18.1271 | 34.5408 |
| cycle 5 | 15.77 | 5 | 25.00 | 78.85 | 20.4235 | 21.6551 |
| cycle 6 | 20.72 | 6 | 36.00 | 124.32 | 22.7199 | 4.00 |
| cycle 7 | 26.37 | 7 | 49.00 | 184.59 | 25.0162 | 1.83267 |
| cycle 8 | 29.88 | 8 | 64.00 | 239.04 | 27.3126 | 6.59152 |
| cycle 9 | 33.32 | 9 | 81.00 | 299.88 | 29.6090 | 13.7718 |
| cycle10 | 37.41 | 10 | 100.00 | 374.10 | 31.9053 | 30.3014 |
| cycle11 | 40.70 | 11 | 121.00 | 447.70 | 34.20 | 42.23 |
| cycle12 | 41.90 | 12 | 144.00 | 502.80 | 36.50 | 29.1809 |
| cycle13 | 45.29 | 13 | 169.00 | 588.77 | 38.7944 | 42.19 |
| cycle14 | 49.89 | 14 | 196.00 | 698.46 | 41.09 | 77.43 |
| cycle15 | 50.59 | 15 | 225.00 | 758.85 | 43.3872 | 51.881 |
| cycle16 | 52.82 | 16 | 256.00 | 845.12 | 45.6835 | 50.9294 |
| cycle17 | 54.46 | 17 | 289.00 | 925.82 | 47.9799 | 41.9919 |
| cycle18 | 55.49 | 18 | 324.00 | 998.82 | 50.2762 | 27.1833 |
| cycle19 | 56.11 | 19 | 361.00 | 1066.09 | 52.5726 | 12.5131 |
| cycle20 | 58.49 | 20 | 400.00 | 1169.80 | 54.8690 | 13.1119 |
| cycle21 | 58.27 | 21 | 441.00 | 1223.67 | 57,1653 | 1.22027 |
| cycle22 | 59.64 | 22 | 484.00 | 1312.08 | 59.4617 | 0.03179 |
| cycle23 | 64.26 | 23 | 529.00 | 1477.98 | 61.76 | 6.25967 |
| cycle24 | 63.50 | 24 | 576.00 | 1524.00 | 64.0544 | 0.31 |
| cycle25 | 63.63 | 25 | 625.00 | 1590.75 | 66.3508 | 7.40274 |
| cycle26 | 64.87 | 26 | 676.00 | 1686.62 | 68.6472 | 14.2669 |
| cycle27 | 65.55 | 27 | 729.00 | 1769.85 | 70.9435 | 29.0901 |
| cycle28 | 66.75 | 28 | 784.00 | 1869.00 | 73.24 | 42.12 |
| cycle29 | 67.84 | 29 | 841.00 | 1967.36 | 75.5363 | 59.2324 |
| cycle30 | 68.90 | 30 | 900.00 | 2067.00 | 77.8326 | 79.7916 |
| TOTALS | 1336.06 | 465.00 | 9455.00 | 25870.0 | 80.1290 | 1028.91 |
| AVERAGE | 44.5353 | 15.50 | 315.167 | 862.334 | 0.00 | 34.2970 |
| | | | | | | (MSE) |

Next period forecast=80.1290Regression line = : Y =8.94 + 2.29636 * XCorrelation coefficient =0.9592287Standard error = 6.06191

File:

AYLOAD:65 & SPEED:3

v

PAYLOAD:65 & SPEED:3

| Method:Li | | ssion/least | | | | |
|-----------|---------|-------------|---------|---------|----------|---------|
| | @D | Period(x) | x^2 | х * у | Forecast | Error^2 |
| cycle 1 | 0.00 | 1 | 1.00 | 0.00 | 20.2583 | 410.40 |
| cycle 2 | 17.89 | 2 | 4.00 | 35.78 | 26.6773 | 77.2168 |
| cycle 3 | 30.53 | 3 | 9.00 | 91.59 | 33.0963 | 6.58577 |
| cycle 4 | 39.11 | 4 | 16.00 | 156.44 | 39.5152 | .164219 |
| cycle 5 | 47.17 | 5 | 25.00 | 235.85 | 45.9342 | 1.52719 |
| cycle 6 | 54.94 | 6 | 36.00 | 329.64 | 52.3532 | 6.69169 |
| cycle 7 | 13.49 | 7 | 49.00 | 94.43 | 58.7721 | 2050.47 |
| cycle 8 | 70.75 | 8 | 64.00 | 566.00 | 65.1911 | 30.9014 |
| cycle 9 | 78.98 | 9 | 81.00 | 710.82 | 71.61 | 54.32 |
| cycle10 | 80.83 | 10 | 100.00 | 808.30 | 78.03 | 7.84544 |
| cycle11 | 93.51 | 11 | 121.00 | 1028.61 | 84.45 | 82.12 |
| cycle12 | 100.66 | 12 | 144.00 | 1207.92 | 90.8670 | 95.9037 |
| cycle13 | 108.38 | 13 | 169.00 | 1408.94 | 97.2859 | 123.078 |
| cycle14 | 115.36 | 14 | 196.00 | 1615.04 | 103.70 | 135.842 |
| cycle15 | 122.68 | -15 | 225.00 | 1840.20 | 110.12 | 157.657 |
| cycle16 | 130.20 | 16 | 256.00 | 2083.20 | 116.543 | 186.519 |
| cycle17 | 133.58 | 17 | 289.00 | 2270.86 | 122.962 | 112.747 |
| cycle18 | 139.43 | 18 | 324.00 | 2509.74 | 129.38 | 100.987 |
| cycle19 | 145.95 | 19 | 361.00 | 2773.05 | 135.800 | 103.028 |
| cycle20 | 149.68 | 20 | 400.00 | 2993.60 | 142.219 | 55.6713 |
| cycle21 | 152.37 | 21 | 441.00 | 3199,77 | 148.638 | 13.9304 |
| cycle22 | 157.39 | 22 | 484.00 | 3462.58 | 155.057 | 5.44 |
| cycle23 | 163.36 | 23 | 529.00 | 3757.28 | 161.476 | 3.55108 |
| cycle24 | 167.97 | 24 | 576.00 | 4031.28 | 167.895 | 0.00570 |
| cycle25 | 172.84 | 25 | 625.00 | 4321.00 | 174.314 | 2.17123 |
| cycle26 | 175.54 | 26 | 676.00 | 4564.04 | 180.732 | 26.96 |
| cycle27 | 179.82 | 27 | 729.00 | 4855.14 | 187.151 | 53.7497 |
| cycle28 | 182.97 | 28 | 784.00 | 5123.16 | 193.57 | 112.369 |
| cycle29 | 186.24 | 29 | 841.00 | 5400.96 | 199.989 | 189.04 |
| cycle30 | 188.38 | 30 | 900.00 | 5651.40 | 206,408 | 325.02 |
| TOTALS | 3400.00 | 465.00 | 9455.00 | 67126.6 | 212.827 | 4531.92 |
| AVERAGE | 113.333 | 15.50 | 315.167 | 2237.55 | 0.00 | 151.064 |
| | | | | r. | | (MSE) |
| | | | | | | |

Next period forecast= 212.827 Regression line = : Y = 13.8394 + 6.41896 * X Correlation coefficient = 0.9763941Standard error = 12.7222



File: AYLOAD:65 & SPEED:5

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| Method:Li | near Regre | ssion/least | squares | | | |
|------------|------------|-------------|---------|---------|----------|---------|
| Methodiati | eD | Period(x) | x^2 | x * y | Forecast | Error^2 |
| cycle 1 | 0.00 | 1 | 1.00 | 0.00 | 6.92 | 47.8989 |
| cycle 2 | 3.99 | 2 | 4.00 | 7.98 | 9.80 | 33.8015 |
| cycle 3 | 8.21 | 3 | 9.00 | 24.63 | 12.6869 | 20.0426 |
| cycle 4 | 12.38 | 4 | 16.00 | 49.52 | 15.57 | 10.1754 |
| cycle 5 | 16.46 | 5 | 25.00 | 82.30 | 18.45 | 3.97 |
| cycle 6 | 22.54 | 6 | 36.00 | 135.24 | 21.3359 | 1.45 |
| cycle 7 | 25.14 | 7 | 49.00 | 175.98 | 24.2189 | .848465 |
| cycle 8 | 29.41 | 8 | 64.00 | 235.28 | 27,1019 | 5.32745 |
| cycle 9 | 31.16 | 9 | 81.00 | 280.44 | 29.9849 | 1.38093 |
| cycle10 | 34.05 | 10 | 100.00 | 340.50 | 32.8679 | 1.39745 |
| cycle11 | 37.41 | 11 | 121.00 | 411.51 | 35.7509 | 2.75275 |
| cycle12 | 42.12 | 12 | 144.00 | 505.44 | 38.6339 | 12.1532 |
| cycle13 | 45.23 | 13 | 169.00 | 587.99 | 41.5168 | 13.7875 |
| cycle14 | 50.82 | 14 | 196.00 | 711.48 | 44.3998 | 41.2184 |
| cycle15 | 50.61 | -15 | 225.00 | 759.15 | 47.2828 | 11.07 |
| cycle16 | 52.29 | 16 | 256.00 | 836.64 | 50.1658 | 4.51207 |
| cycle17 | 57.02 | 17 | 289,00 | 969.34 | 53.0488 | 15.7702 |
| cycle18 | 59.66 | 18 | 324.00 | 1073.88 | 55.9318 | 13.8993 |
| cycle19 | 60.16 | 19 | 361.00 | 1143.04 | 58.8148 | 1.8095 |
| cycle20 | 64.91 | 20 | 400.00 | 1298.20 | 61.6978 | 10.3181 |
| cycle21 | 65.35 | 21 | 441.00 | 1372.35 | 64.5808 | 0.59 |
| cycle22 | 69.02 | 22 | 484.00 | 1518.44 | 67.4638 | 2.42 |
| cycle23 | 70.53 | 23 | 529.00 | 1622.19 | 70.3468 | 0.03356 |
| cycle24 | 72.89 | 24 | 576.00 | 1749.36 | 73.2298 | .115463 |
| cycle25 | 74.76 | 25 | 625.00 | 1869.00 | 76.11 | 1.83004 |
| cycle26 | 77.68 | 26 | 676.00 | 2019.68 | 79.00 | 1.73 |
| cycle27 | 78.61 | 27 | 729.00 | 2122.47 | 81.8788 | 10.6849 |
| cycle28 | 81.24 | 28 | 784.00 | 2274.72 | 84.7618 | 12.4029 |
| cycle29 | 82.80 | 29 | 841.00 | 2401.20 | 87.6448 | 23.4718 |
| cycle30 | 85.28 | 30 | 900.00 | 2558.40 | 90.5278 | 27.5391 |
| TOTALS | 1461.73 | 465.00 | 9455.00 | 29136.3 | 93.4108 | 334.408 |
| AVERAGE | 48.7243 | 15.50 | 315.167 | 971.212 | 0.00 | 11.1469 |
| | | | | | | (MSE) |

Next period forecast= 93.4108 Regression line = : Y = 4.03791 + 2.88300 * X Correlation coefficient = 0.9911672Standard error = 3.455884 File: AYLOAD:65 & SPEED:7

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PAYLOAD:65 & SPEED:7

| Wethod . I in | noar Dogro | ssion/least | canaros | | | |
|---------------|-------------|-------------|---------|---------|----------|---------|
| Mechou.ht | liear Regre | Period(x) | x^2 | x * y | Forecast | Error^2 |
| cycle 1 | 0.00 | 1 | 1.00 | 0.00 | 25.3003 | 640.104 |
| cycle 2 | 18.84 | 2 | 4.00 | 37.68 | 29.1574 | 106.448 |
| cycle 3 | 28.47 | 3 | 9.00 | 85.41 | 33.0144 | 20.6519 |
| cycle 4 | 34.61 | 4 | 16.00 | 138.44 | 36.8715 | 5.11447 |
| cycle 5 | 38.92 | 5 | 25.00 | 194.60 | 40.7286 | 3.27107 |
| cycle 6 | 42.29 | 6 | 36.00 | 253.74 | 44.59 | 5.27 |
| cycle 7 | 46.21 | 7 | 49.00 | 323.47 | 48.4428 | 4.98529 |
| cycle 8 | 50.10 | 8 | 64.00 | 400.80 | 52.2999 | 4.84 |
| cycle 9 | 52.75 | 9 | 81.00 | 474.75 | 56.1569 | 11.6073 |
| cycle10 | 65.16 | 10 | 100.00 | 651.60 | 60.01 | 26.48 |
| cycle11 | 71.77 | 11 | 121.00 | 789.47 | 63.8711 | 62.3923 |
| cycle12 | 76.82 | 12 | 144.00 | 921.84 | 67.7282 | 82.6608 |
| cycle13 | 81.17 | 13 | 169.00 | 1055.21 | 71.59 | 91.8667 |
| cycle14 | 86.38 | 14 | 196.00 | 1209.32 | 75.4424 | 119.632 |
| cycle15 | 91.35 | 15 | 225.00 | 1370.25 | 79.2995 | 145.216 |
| cycle16 | 95.47 | 16 | 256.00 | 1527.52 | 83.1565 | 151.621 |
| cycle17 | 97.89 | 17 | 289.00 | 1664.13 | 87.0136 | 118.295 |
| cycle18 | 102.01 | 18 | 324.00 | 1836.18 | 90.8707 | 124.084 |
| cycle19 | 102.95 | 19 | 361.00 | 1956.05 | 94.73 | 67.6047 |
| cycle20 | 104.70 | 20 | 400.00 | 2094.00 | 98.5849 | 37.39 |
| cycle21 | 106.36 | 21 | 441.00 | 2233.56 | 102.442 | 15.35 |
| cycle22 | 108.28 | 22 | 484.00 | 2382.16 | 106.299 | 3.92416 |
| cycle23 | 111.11 | 23 | 529.00 | 2555.53 | 110.156 | .909859 |
| cycle24 | 111.84 | 24 | 576.00 | 2684.16 | 114.013 | 4.72288 |
| cycle25 | 112.67 | 25 | 625.00 | 2816,75 | 117.87 | 27.0431 |
| cycle26 | 115.54 | 26 | 676.00 | 3004.04 | 121.727 | 38.2837 |
| cycle27 | 117.96 | 27 | 729.00 | 3184.92 | 125.584 | 58.1326 |
| cycle28 | 120.03 | 28 | 784.00 | 3360.84 | 129.442 | 88.5775 |
| cycle29 | 122.30 | 29 | 841.00 | 3546.70 | 133.299 | 120.97 |
| cycle30 | 122.89 | 30 | 900.00 | 3686.70 | 137.156 | 203.511 |
| TOTALS | 2436.84 | 465.00 | 9455.00 | 46439.8 | 141.013 | 2390.97 |
| AVERAGE | 81.228 | 15.50 | 315.167 | 1547.99 | 0.00 | 79.6988 |
| | | | | | | (MSE) |

Next period forecast= 141.013 Regression line = : Y = 21.4432 + 3.85708 * X Correlation coefficient = 0.9660556Standard error = 9.240759

File: PAYLOAD:130 & SPEED:3 PAYLOAD:130 & SPEED:3

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| ethod.I i | noor Boaro | ssion/least | eallaroc | | | |
|------------|------------|-------------|----------------|-------------|----------|---------|
| Method: DI | | Period(x) | x ² | x * y | Forecast | Error^2 |
| cycle 1 | 0.00 | 1 | 1.00 | 0.00 | 22.7515 | 517.629 |
| cycle 2 | 9.00 | 2 | 4.00 | 18.00 | 24.6077 | 243.599 |
| cycle 3 | 11.91 | 3 | 9.00 | 35.73 | 26.4639 | 211.81 |
| cycle 4 | 17.87 | 4 | 16.00 | 71.48 | 28.32 | 109.204 |
| cycle 5 | 24.70 | 5 | 25.00 | 123.50 | 30,1763 | 29.9894 |
| cycle 6 | 32.31 | 6 | 36.00 | 193.86 | 32.0325 | 0.07703 |
| cycle 7 | 37.61 | 7 | 49.00 | 263.27 | 33.8887 | 13.8484 |
| cycle 8 | 44.31 | 8 | 64.00 | 354.48 | 35.7449 | 73.3618 |
| cycle 9 | 49.96 | 9 | 81.00 | 449.64 | 37.60 | 152.744 |
| cycle10 | 52.50 | 10 | 100.00 | 525.00 | 39.4572 | 170.113 |
| cycle11 | 53.99 | 11 | 121.00 | 593.89 | 41.3134 | 160.695 |
| cycle12 | 42.72 | 12 | 144.00 | 512.64 | 43.1696 | .202175 |
| cycle13 | 66.01 | 13 | 169.00 | 858.13 | 45.0258 | 440.335 |
| cycle14 | 52.20 | 14 | 196.00 | 730.80 | 46.88 | 28.2808 |
| cycle15 | 66.88 | 15 | 225.00 | 1003.20 | 48.7382 | 329.124 |
| cycle16 | 53.70 | 16 | 256.00 | 859.20 | 50.5944 | 9.64458 |
| cycle17 | 52.96 | 17 | 289.00 | 900.32 | 52.4506 | .259457 |
| cycle18 | 53.15 | 18 | 324.00 | 956.70 | 54.3068 | 1.33825 |
| cycle19 | 53.36 | 19 | 361.00 | 1013.84 | 56.16 | 7.85695 |
| cycle20 | 55.18 | 20 | 400.00 | 1103.60 | 58.0192 | 8.06118 |
| cycle21 | 70.91 | 21 | 441.00 | 1489.11 | 59.8754 | 121.762 |
| cycle22 | 69.16 | 22 | 484.00 | 1521.52 | 61.7316 | 55.1809 |
| cycle23 | 68.38 | 23 | 529.00 | 1572.74 | 63.5878 | 22.97 |
| cycle24 | 66.80 | 24 | 576.00 | 1603.20 | 65.44 | 1.83872 |
| cycle25 | 69.61 | 25 | 625.00 | 1740.25 | 67.3002 | 5.33514 |
| cycle26 | 67.98 | 26 | 676.00 | 1767.48 | 69.1564 | 1.38392 |
| cycle27 | 69.59 | 27 | 729.00 | 1878.93 | 71.0126 | 2.02381 |
| cycle28 | 68.37 | 28 | 784.00 | 1914.36 | 72.8688 | 20.2392 |
| cycle29 | 54.32 | 29 | 841.00 | 1575.28 | 74.725 | 416.364 |
| cycle30 | 54.55 | 30 | 900.00 | 1636.50 | 76.58 | 485.373 |
| TOTALS | 1489.99 | 465.00 | 9455.00 | 27266.6 | 78.44 | 3640.65 |
| AVERAGE | 49.6663 | 15.50 | 315.167 | 908.888 | 0.00 | 121.355 |
| | | | | - | | (MSE) |
| | | | Next perio | 1 forecast= | 78.44 | |

Next period forecast=78.44Regression line = : Y = 20.8953 + 1.85620 * X Correlation coefficient = 0.8247457Standard error = 11.40276 File: AYLOAD:130 & SPEED:5

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PAYLOAD:130 & SPEED:5

| Method:Lin | near Regre | ssion/least | squares | | | |
|------------|------------|-------------|---------|---------|----------|---------|
| | @D | Period(x) | x^2 | х * у | Forecast | Error^2 |
| cycle 1 | 0.00 | 1 | 1.00 | 0.00 | 23.8771 | 570.12 |
| cycle 2 | 18.23 | 2 | 4.00 | 36.46 | 27.3993 | 84.0768 |
| cycle 3 | 27.54 | 3 | 9.00 | 82.62 | 30.9216 | 11.4350 |
| cycle 4 | 30.17 | 4 | 16.00 | 120.68 | 34.44 | 18.2653 |
| cycle 5 | 28.38 | 5 | 25.00 | 141.90 | 37.97 | 91.8915 |
| cycle 6 | 31.58 | 6 | 36.00 | 189.48 | 41.4882 | 98.1730 |
| cycle 7 | 38.14 | 7 | 49.00 | 266.98 | 45.0104 | 47.20 |
| cycle 8 | 51.87 | 8 | 64.00 | 414.96 | 48.5327 | 11.1378 |
| cycle 9 | 58.57 | 9 | 81.00 | 527.13 | 52.05 | 42.4466 |
| cycle10 | 63.51 | 10 | 100.00 | 635.10 | 55.5771 | 62.9307 |
| cycle11 | 71.48 | 11 | 121.00 | 786.28 | 59.0993 | 153.281 |
| cycle12 | 75.54 | 12 | 144.00 | 906.48 | 62.6216 | 166.886 |
| cycle13 | 77.69 | 13 | 169.00 | 1009.97 | 66.1438 | 133.315 |
| cycle14 | 79.16 | 14 | 196.00 | 1108.24 | 69.666 | 90.1361 |
| cycle15 | 83.50 | 15 | 225.00 | 1252.50 | 73.1882 | 106.333 |
| cycle16 | 86.20 | 16 | 256.00 | 1379.20 | 76.7104 | 90.0517 |
| cycle17 | 88.93 | 17 | 289.00 | 1511.81 | 80.2327 | 75.6436 |
| cycle18 | 91.74 | 18 | 324.00 | 1651.32 | 83.7549 | 63.76 |
| cycle19 | 93.09 | 19 | 361.00 | 1768.71 | 87.2771 | 33.7897 |
| cycle20 | 98.24 | 20 | 400.00 | 1964.80 | 90.7993 | 55.3635 |
| cycle21 | 98.28 | 21 | 441.00 | 2063.88 | 94.3215 | 15.6693 |
| cycle22 | 100.40 | 22 | 484.00 | 2208.80 | 97.8438 | 6.53 |
| cycle23 | 101.52 | 23 | 529.00 | 2334.96 | 101.366 | 0.02 |
| cycle24 | 103.89 | 24 | 576.00 | 2493.36 | 104.888 | .996433 |
| cycle25 | 106.38 | 25 | 625.00 | 2659.50 | 108.41 | 4.12269 |
| cycle26 | 106.89 | 26 | 676.00 | 2779.14 | 111.933 | 25.4285 |
| cycle27 | 108.79 | 27 | 729.00 | 2937.33 | 115.45 | 44.4206 |
| cycle28 | 108.46 | 28 | 784.00 | 3036.88 | 118.977 | 110.609 |
| cycle29 | 110.14 | 29 | 841.00 | 3194.06 | 122.499 | 152.753 |
| cycle30 | 110.17 | 30 | 900.00 | 3305.10 | 126.022 | 251.272 |
| TOTALS | 2248.48 | 465.00 | 9455.00 | 42767.6 | 129.544 | 2618.07 |
| AVERAGE | 74.9493 | 15.50 | 315.167 | 1425.59 | 0.00 | 87.2689 |
| | | | | | | (MSE) |

Next period forecast=129.544Regression line = : Y = 20.3549 + 3.52222 * XCorrelation coefficient =0.9561192Standard error = 9.669665

File: AYLOAD:130 & SPEED:7

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PAYLOAD:130 & SPEED:7

| | ~ | | | | | |
|-----------|-----------|-------------|---------|---------|----------|---------|
| Method:L1 | | ssion/least | | | | - |
| _ | | Period(x) | x^2 | х * у | Forecast | Error^2 |
| cycle 1 | 0.00 | 1 | 1.00 | 0.00 | 11.8843 | 141.237 |
| cycle 2 | 4.75 | 2 | 4.00 | 9.50 | 18.2446 | 182.103 |
| cycle 3 | 21.26 | 3 | 9.00 | 63.78 | 24.60 | 11.1876 |
| cycle 4 | 30.54 | 4 | 16.00 | 122.16 | 30.97 | 0.18 |
| cycle 5 | 37.84 | 5 | 25.00 | 189.20 | 37.3252 | .264973 |
| cycle 6 | 44.84 | 6 | 36.00 | 269.04 | 43.6855 | 1.33293 |
| cycle 7 | 49.53 | 7 | 49.00 | 346.71 | 50.0457 | .265952 |
| cycle 8 | 54.72 | 8 | 64.00 | 437.76 | 56.4059 | 2.84237 |
| cycle 9 | 60.38 | 9 | 81.00 | 543.42 | 62.7662 | 5.69377 |
| cycle10 | 65.73 | 10 | 100.00 | 657.30 | 69.13 | 11.5354 |
| cycle11 | 72.90 | 11 | 121.00 | 801.90 | 75.4866 | 6.69059 |
| cycle12 | 80.84 | 12 | 144.00 | 970.08 | 81.8468 | 1.01 |
| cycle13 | 87.04 | 13 | 169.00 | 1131.52 | 88.21 | 1.36207 |
| cycle14 | 94.69 | 14 | 196.00 | 1325.66 | 94.5673 | 0.02 |
| cycle15 | 103.54 | 15 | 225.00 | 1553.10 | 100.928 | 6.82497 |
| cycle16 | 110.40 | 16 | 256.00 | 1766.40 | 107.288 | 9.68601 |
| cycle17 | 116.41 | 17 | 289.00 | 1978.97 | 113.648 | 7.62869 |
| cycle18 | 144.95 | 18 | 324.00 | 2609.10 | 120.008 | 622.092 |
| cycle19 | 148.60 | 19 | 361.00 | 2823.40 | 126.368 | 494.24 |
| cycle20 | 152.08 | 20 | 400.00 | 3041.60 | 132.729 | 374.474 |
| cycle21 | 154.63 | 21 | 441.00 | 3247.23 | 139.09 | 241.526 |
| cycle22 | 156.35 | 22 | 484.00 | 3439.70 | 145.449 | 118.829 |
| cycle23 | 159.17 | 23 | 529.00 | 3660.91 | 151.809 | 54.1788 |
| cycle24 | 159.69 | 24 | 576.00 | 3832.56 | 158.170 | 2.31 |
| cycle25 | 162.15 | 25 | 625.00 | 4053.75 | 164.530 | 5.66362 |
| cycle26 | 164.98 | 26 | 676.00 | 4289.48 | 170.89 | 34.9289 |
| cycle27 | 167.99 | 27 | 729.00 | 4535.73 | 177.25 | 85.7529 |
| cycle28 | 169.87 | 28 | 784.00 | 4756.36 | 183.61 | 188.802 |
| cycle29 | 172.45 | 29 | 841.00 | 5001.05 | 189.97 | 306.977 |
| cycle30 | 174.91 | 30 | 900.00 | 5247.30 | 196.331 | 458.858 |
| TOTALS | 3123.23 | 465.00 | 9455.00 | 62704.7 | 202.691 | 3378.50 |
| AVERAGE | 104.108 - | | 315.167 | 2090.16 | 0.00 | 112.617 |
| | | | | | | (MSE) |
| | | | | | | |

Next period forecast=202.691Regression line = : Y =5.52 +6.36 * XCorrelation coefficient =0.9819223Standard error = 10.98457

File: AYLOAD:180 & SPEED:3

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PAYLOAD:180 & SPEED:3

| Method:Li | near Regres | sion/least | squares | | | |
|-----------|-------------|------------|---------|---------|----------|---------|
| | ēd | Period | x^2 | х * у | Forecast | Error^2 |
| cycle 1 | 0.00 | 1 | 1.00 | ō.00 | 38,3746 | 1472.61 |
| cycle 2 | 15.94 | 2 | 4.00 | 31.88 | 38.8281 | 523.866 |
| cycle 3 | 29.00 | 3 | 9.00 | 87.00 | 39.2817 | 105.712 |
| cycle 4 | 43.53 | 4 | 16.00 | 174.12 | 39.7352 | 14.4004 |
| cycle 5 | 45.83 | 5 | 25.00 | 229.15 | 40.1888 | 31.8237 |
| cycle 6 | 50.09 | 6 | 36.00 | 300.54 | 40.6423 | 89.26 |
| cycle 7 | 50.22 | 7 | 49.00 | 351.54 | 41.0958 | 83.2502 |
| cycle 8 | 50.23 | 8 | 64.00 | 401.84 | 41.55 | 75.3529 |
| cycle 9 | 48.62 | 9 | 81.00 | 437.58 | 42.0029 | 43.7855 |
| cycle10 | 50.32 | 10 | 100.00 | 503.20 | 42.46 | 61.83 |
| cycle11 | 52.21 | 11 | 121.00 | 574.31 | 42.91 | 86.4893 |
| cycle12 | 53.61 | 12 | 144.00 | 643.32 | 43.3636 | 104.989 |
| cycle13 | 55.42 | 13 | 169.00 | 720.46 | 43.8171 | 134.627 |
| cycle14 | 54.32 | 14 | 196.00 | 760.48 | 44.2707 | 100.99 |
| cycle15 | 51.15 | 15 | 225.00 | 767.25 | 44.7242 | 41.2906 |
| cycle16 | 47.32 | 16 | 256.00 | 757.12 | 45.1778 | 4.58914 |
| cycle17 | 50.25 | 17 | 289.00 | 854.25 | 45.6313 | 21.3322 |
| cycle18 | 47.32 | 18 | 324.00 | 851.76 | 46.0849 | 1.52556 |
| cycle19 | 47.51 | 19 | 361.00 | 902.69 | 46.5384 | .943976 |
| cycle20 | 48.80 | 20 | 400.00 | 976.00 | 46.9920 | 3.26901 |
| cycle21 | 47.80 | 21 | 441.00 | 1003.80 | 47.4455 | .125665 |
| cycle22 | 48.66 | 22 | 484.00 | 1070.52 | 47.90 | .579036 |
| cycle23 | 47.56 | 23 | 529.00 | 1093.88 | 48.3526 | .628213 |
| cycle24 | 44.91 | 24 | 576.00 | 1077.84 | 48.8061 | 15.1800 |
| cycle25 | 46.31 | 25 | 625.00 | 1157.75 | 49.2597 | 8.70 |
| cycle26 | 47.33 | 26 | 676.00 | 1230.58 | 49.7132 | 5.67983 |
| cycle27 | 43.94 | 27 | 729.00 | 1186.38 | 50.17 | 38.7729 |
| cycle28 | 44.70 | 28 | 784.00 | 1251.60 | 50.6203 | 35.0504 |
| cycle29 | 44.18 | 29 | 841.00 | 1281.22 | 51.0739 | 47.5256 |
| cycle30 | 41.45 | 30 | 900.00 | 1243.50 | 51.5274 | 101.555 |
| TOTALS | 1348.53 | 465.00 | 9455.00 | 21921.6 | 51.9810 | 3255.73 |
| AVERAGE | 44.951 - | 15.50 | 315.167 | 730.719 | 0.00 | 108.524 |
| | | | | | | (MSE) |

Next period forecast=51.9810Regression line = : Y =37.92 + .453547 * XCorrelation coefficient =0.3526257Standard error = 10.78314

File: AYLOAD:180 & SPEED:5 PAYLOAD:180 & SPEED:5

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| Method:Linea | r Reares | sion/least | squares | | | |
|--------------|----------|------------|---------|---------|----------|---------|
| | @D | Period | x^2 | x * y | Forecast | Error^2 |
| cycle 1 | 0.00 | 1 | 1.00 | 0.00 | 4.01796 | 16.1440 |
| cycle 2 | 5.80 | 2 | 4.00 | 11.60 | 4.05539 | 3.04 |
| cycle 3 | 5.24 | 3 | 9.00 | 15.72 | 4.09281 | 1.31604 |
| cycle 4 | 9.49 | 4 | 16.00 | 37.96 | 4.13024 | 28.727 |
| cycle 5 | 2.16 | 5 | 25.00 | 10.80 | 4.16767 | 4.03074 |
| cycle 6 | 1.73 | 6 | 36.00 | 10.38 | 4.21 | 6.12611 |
| cycle 7 | 1.95 | 7 | 49.00 | 13.65 | 4.24253 | 5.25568 |
| cycle 8 | 6.74 | 8 | 64.00 | 53.92 | 4.27995 | 6.05182 |
| cycle 9 | 6.93 | 9 | 81.00 | 62.37 | 4.31738 | 6.82577 |
| cycle10 | 6.34 | 10 | 100.00 | 63.40 | 4.35481 | 3.94097 |
| cycle11 | 3.84 | 11 | 121.00 | 42.24 | 4.39224 | .304969 |
| cycle12 | 4.03 | 12 | 144.00 | 48.36 | 4.42967 | .159734 |
| cycle13 | 3.23 | 13 | 169.00 | 41.99 | 4.46710 | 1.53 |
| cycle14 | 3.79 | 14 | 196.00 | 53.06 | 4.50452 | .510545 |
| cycle15 | 2.64 | 15 | 225.00 | 39.60 | 4.54195 | 3.61742 |
| cycle16 | 2.79 | 16 | 256.00 | 44.64 | 4.57938 | 3.20188 |
| cycle17 | 7.58 | 17 | 289.00 | 128.86 | 4.62 | 8.78 |
| cycle18 | 3.75 | 18 | 324.00 | 67.50 | 4.65424 | .817645 |
| cycle19 | 3.81 | 19 | 361.00 | 72.39 | 4.69167 | .777334 |
| cycle20 | 3.74 | 20 | 400.00 | 74.80 | 4.72909 | .978306 |
| cycle21 | 3.87 | 21 | 441.00 | 81.27 | 4.76652 | .803752 |
| cycle22 | 3.60 | 22 | 484.00 | 79.20 | 4.80395 | 1.44950 |
| cycle23 | 7.41 | 23 | 529.00 | 170.43 | 4.84138 | 6.59782 |
| cycle24 | 6.74 | 24 | 576.00 | 161.76 | 4.88 | 3.46404 |
| cycle25 | 4.85 | 25 | 625.00 | 121.25 | 4.91623 | 0.00439 |
| cycle26 | 4.26 | 26 | 676.00 | 110.76 | 4.95366 | 0.48 |
| cycle27 | 4.98 | 27 | 729.00 | 134.46 | 4.99109 | 0.00 |
| cycle28 | 4.35 | 28 | 784.00 | 121.80 | 5.03 | .460388 |
| cycle29 | 4.74 | 29 | 841.00 | 137.46 | 5.06595 | 0.11 |
| cycle30 | 6.44 | 30 | 900.00 | 193.20 | 5.10338 | 1.78657 |
| | 136.82 | 465.00 | 9455.00 | 2204.83 | 5.14 | 117.295 |
| AVERAGE 4 | .56067 - | 15.50 | 315.167 | 73.4943 | 0.00 | 3.90982 |
| | | | | | | (MSE) |

Next period forecast=5.14Regression line = : Y = 3.98053 + .037428 * XCorrelation coefficient =0.1616808Standard error = 2.046727

File: AYLOAD:250 & SPEED:3

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| Method:Li | near Regress | sion/least | squares | | | |
|------------|--------------|------------|---------|---------|----------|---------|
| 1001104121 | êD | Period | x^2 | x * y | Forecast | Error^2 |
| cycle 1 | 0.00 | 1 | 1.00 | 0.00 | 13.10 | 171.584 |
| cycle 2 | 1.22 | 2 | 4.00 | 2.44 | 13,2983 | 145.885 |
| cycle 3 | 8.22 | 3 | 9.00 | 24.66 | 13.4976 | 27.85 |
| cycle 4 | 14.80 | 4 | 16.00 | 59.20 | 13.6969 | 1.21693 |
| cycle 5 | 17.33 | 5 | 25.00 | 86.65 | 13.8961 | 11.79 |
| cycle 6 | 19.21 | 6 | 36.00 | 115.26 | 14.0954 | 26.1588 |
| cycle 7 | 22.33 | 7 | 49.00 | 156.31 | 14.2947 | 64.5658 |
| cycle 8 | 22.19 | 8 | 64.00 | 177.52 | 14.49 | 59.2283 |
| cycle 9 | 23.18 | 9 | 81.00 | 208.62 | 14.69 | 72.02 |
| cycle10 | 21.48 | 10 | 100.00 | 214.80 | 14.8926 | 43.39 |
| cycle11 | 21.30 | 11 | 121.00 | 234.30 | 15.0919 | 38.5409 |
| cycle12 | 18.78 | 12 | 144.00 | 225.36 | 15.2912 | 12.17 |
| cycle13 | 16.75 | 13 | 169.00 | 217.75 | 15.4904 | 1.58648 |
| cycle14 | 15.63 | 14 | 196.00 | 218.82 | 15.6897 | 0.00357 |
| cycle15 | 14.55 | 15 | 225.00 | 218.25 | 15.89 | 1.79 |
| cycle16 | 16.16 | 16 | 256.00 | 258.56 | 16.0883 | .005139 |
| cycle17 | 13.87 | 17 | 289.00 | 235.79 | 16.2876 | 5.84 |
| cycle18 | 13.61 | 18 | 324.00 | 244.98 | 16.49 | 8.27648 |
| cycle19 | 13.57 | 19 | 361.00 | 257.83 | 16.6862 | 9.71054 |
| cycle20 | 14.58 | 20 | 400.00 | 291.60 | 16.8855 | 5.31515 |
| cycle21 | 13.64 | 21 | 441.00 | 286.44 | 17.0848 | 11.8663 |
| cycle22 | 13.84 | 22 | 484.00 | 304.48 | 17.28 | 11.8614 |
| cycle23 | 14.98 | 23 | 529.00 | 344.54 | 17.4833 | 6.26664 |
| cycle24 | 13.56 | 24 | 576.00 | 325.44 | 17.6826 | 16.9960 |
| cycle25 | 18.56 | 25 | 625.00 | 464.00 | 17.8819 | .459815 |
| cycle26 | 18.21 | 26 | 676.00 | 473.46 | 18.08 | 0.01659 |
| cycle27 | 18.21 | 27 | 729.00 | 491.67 | 18.2805 | 0.00 |
| cycle28 | 17.82 | 28 | 784.00 | 498.96 | 18.4798 | .435293 |
| cycle29 | 17.46 | 29 | 841.00 | 506.34 | 18.68 | 1.48610 |
| cycle30 | 24.62 | 30 | 900.00 | 738.60 | 18.8783 | 32.9666 |
| TOTALS | 479.66 | 465.00 | 9455.00 | 7882.63 | 19.0776 | 789.308 |
| AVERAGE | 15.9887 - | 15.50 | 315.167 | 262.754 | 0.00 | 26.3103 |
| | | | | | | (MSE) |

Next period forecast= 19.0776 Regression line = : Y = 12.8997 + .199288 * X Correlation coefficient = 0.3187449Standard error = 5.309386